Experimental- theoretical study of Spray combustion in the small Jet Engines

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DEVELOPMENT OF ATOMIZATION SYSTEMFOR SMALL JET ENGINES (T<1000Nt)

Olympus (AMT)



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The work included the following stages

- Experimental study of the atomization. 1.
- Development of the air-blast atomizers with 2. axial and radial air swirlers.
- 3. Spray Dynamics study by CFD.
- 4. Preliminary combustion study with the air-blast atomizers





Development of the air-blast atomizers with axial and radial air swirlers.





Axial air swirler dimensions:

Vanes inclination: 45°

Swirler OD: 13 mm

Swirler ID: 7 mm

Liquid nozzle assembly OD: 6mm

Radial air swirler dimensions: OD: 14 mm, ID: 8 mm, Vanes Height: 1.5 mm, Ring Cover Thickness: 1 mm.

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4 Air-assist atomizer with axial air swirler



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TASK: TO DEVELOPE A WIDE ANGLE ATOMIZER WITH SMALL DROPLETS

By the study of:

- 1. Liquid bubble dynamics and sheet and droplets performance.
- 2. Pressure field at the atomizer exit.

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TEST CONDITIONS:

Liquid and air have co-rotated direction (for better atomization),

air pressure drop:0 - 0.1 bars,water pressure drop:1.2 - 6 bars,air / liquid mass flow ratio: 1 - 4.

Exit velocity (at exit cross-section): 10 m/s to 40 m/s for the axial air swirler 40 m/s to 115 m/s for the radial. Both, water and kerosene were used.



PHASE DOPPLER ANEMOMETER FOR MEASURING:

- droplet size,
- axial velocity (droplets and air),
- liquid flux







spray is opened due to static pressure difference
The spray angle can become very large (Even at low air velocity < 20 m/s)
This phenomena enables to achieve large cone

angle (>120°) and provides fine atomization.

• This effect was not described earlier.

• We now try to use it in our small combustor design where fuel pressure should be very low.









Spray cone at the simplex atomizer, $\Delta P_L = 5$ bars.

AXIAL SWIRLER



Atomization modes, (a) $\Delta P_L = 1.4$ bars, $\Delta P_A = 0$; (b) $\Delta P_L = 1.4$ bars, $\Delta P_A = 0.76$ millibar.



Atomization modes, (a) $\Delta P_L = 1.7$ bars, $\Delta P_A = 0$; (b) $\Delta P_L = 1.7$ bars, $\Delta P_A = .51$ millibar;

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Fuel

Cone angle, air-assist atomizer



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Step-shaped change of droplet size with air velocity

The collapse of jet takes place even at the low liquid pressure drop and at the low air velocity

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SMD comparison for kerosene and water



CFD SIMULATION







A 60° sector view at STAR-CD. 5 solid cell types with 18,948 cells 32 fluid cell types with 525,35 cells 436,11 tetrahedrals, 92,767 hexahedrals, 14,833 pyramids 184,478 vertices, 22,675 boundary cells

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Turbo and Jet Engine Laboratory Technion – Israel jet-engine-lab.technion.ac.il Air Inlet: =0.485 kg/sec, T_{03} =498 K P_{03} = 0.425 Mpa, ρ =2.923 kg/m³ Fixed mass flux boundary condition. **Fuel Inlet** (propane): m =0.011 kg/sec (for the whole combustor) T =373 ° K ρ =6.013 kg/m³ Fixed mass flux boundary condition. **Solid:** $k = 43 \text{ W/(m K)} \rho = 7800 \text{ kg/m}^3 \text{ Cp} = 473 \text{ KJ/(kg K)}$ **Turbulence Model:** k-Epsilon/High Reynolds Number **Chemical Reaction Type:** Non-premixed **Reaction Model:** Hybrid EBU/Chemical kinetics **Reaction System** (propane fuel, Two steps reaction): $C_3H_8 + 3.5O_2 \rightarrow 3CO + 4H_2O$ $CO + 0.5O, \rightarrow CO,$ Solution Method: Steady State SIMPLE **Differencing Schemes: MARS**

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Simulation conditions





Velocity field at the second lengthwise section, (cold flow)



NEAR WALL GAS TEMPERATURE



WALL (METAL) TEMPERATURE











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ATOMIZATION STUDY BY CFD Mesh building: SOLID WORKS, STAR DESIGN



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CFD SIMULATION WITHOUT SWIRLER

Generic atomizer

Heptane (C_7H_{16}) was used as a fuel Fuel temperature was 300 K. The fuel /air ratio was equaled to 0.01 Mono-size spray with droplet diameter of 30 microns. Droplet velocity was equal 42 m/s Total spray cone is equal to 90^o Secondary break-up simulation (Reitz and Diwakar model)

Laminar and turbulent flows are simulated

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SPRAY TRAJECTORIES, TURBULENT FLOW

Spray is pressed against inlet wall due to reverse air.



longitudinal section

cross section

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SPRAY – VORTEX INTERACTION









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Droplets' combustion



Reverse flow drags droplets backwards

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PRELIMINARY STUDY OF THE COMBUSTOR WITH THE AIR-BLAST ATOMIZERS

Atomization process inside a combustor - Transparent combustor model.

1. GASTURB simulations (combustor operational regime).

2. Modification of holes (number, diameter and swirler size).

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ATOMIZATION PROCESS INSIDE A COMBUSTOR

The "OLYMPUS" combustor was modified (number & diameter of holes in primary ZONE)





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General view of the modified combustor



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PRELIMINARY TEST RESULTS:

Modification of holes number, their diameter and swirler size.



Test showed that the original primary zone is not adequate to accommodate the swirl atomizers result was incomplete combustion.

Fuel burns downstream of combustor

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We assumed that the reason is excess air and high air velocities at the primary zone: swirler air flow rate \rightarrow decreased

 $D_{holes} \rightarrow Increased$ N _{holes} $\rightarrow Increased$.





Modified combustor, open exit

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Combustion test



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Test ignition and combustion



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Test with open exit of the combustor



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Tests demonstrated stable combustion over a wide range of fuel and air flow rates



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Test with turbine vanes at the exit



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Ignition process, turbine stator is installed



successful Ignition was achieved for the following parameters: Ta = 298 K, P=1 bar m_a (max) = 0.147 kg/s m_f = 0.0032 – 0.0063 kg/s (f = 0.022-0.043)

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COMBUSTION TESTS





Combustion, open exit



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Test Conditions:: 298 K Ambient temperature = Combustion pressure = 1bar Supply pressure = 1.1 bar Air flow rate (max) = 0.180 kg/s Fuel flow rate = 3.2 - 6.3 gr/s (f = 0.018 - 0.035)

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CONCLUSIONS

Fuel system for small combustor with 6 air-blast atomizers was developed. 9

1. Air-blast atomizer: the collapse of Liquid bubble generates wide angle and fine spray at low pressures

 Fine spray (SMD of 30-50 microns) is feasible even at low liquid pressure (<1 bar) and low air velocity (<30 m/s).

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CONCLUSION (cont.)

2. ATOMIZATION AND COMBUSTION STUDY BY CFD.

As CFD simulations cannot take into account evolution of liquid bubble and its collapse.

Yet, only qualitative agreement was found between simulations and experiment.

3. TEST-RIG AND COMBUSTION TESTS:

The liner of "OLYMPUS" combustor with transparent casing was used as prototype.

Modification in the combustor included variations in the swirlers and holes of the primary zone.

The modified combustor was successfully tested and spark ignition within wide range of air and fuel flow rates was achieved.

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