

**STEADY-STATE / TRANSIENT
SIMULATIONS AND CONTROL
OF SINGLE-SPOOL JET ENGINES**

by

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1. Steady-State / Dynamic

Mathematical Model

2. MATLAB Program DYNJET-D1:

Steady-State Calculations

3. SIMULINK Program DYNJET-D3:

Transient Response Simulations

4. Feed-Back Nonlinear Control for the Single-Spool Engine

4.1. The Control System

Specifications

4.2. Nonlinear Controller

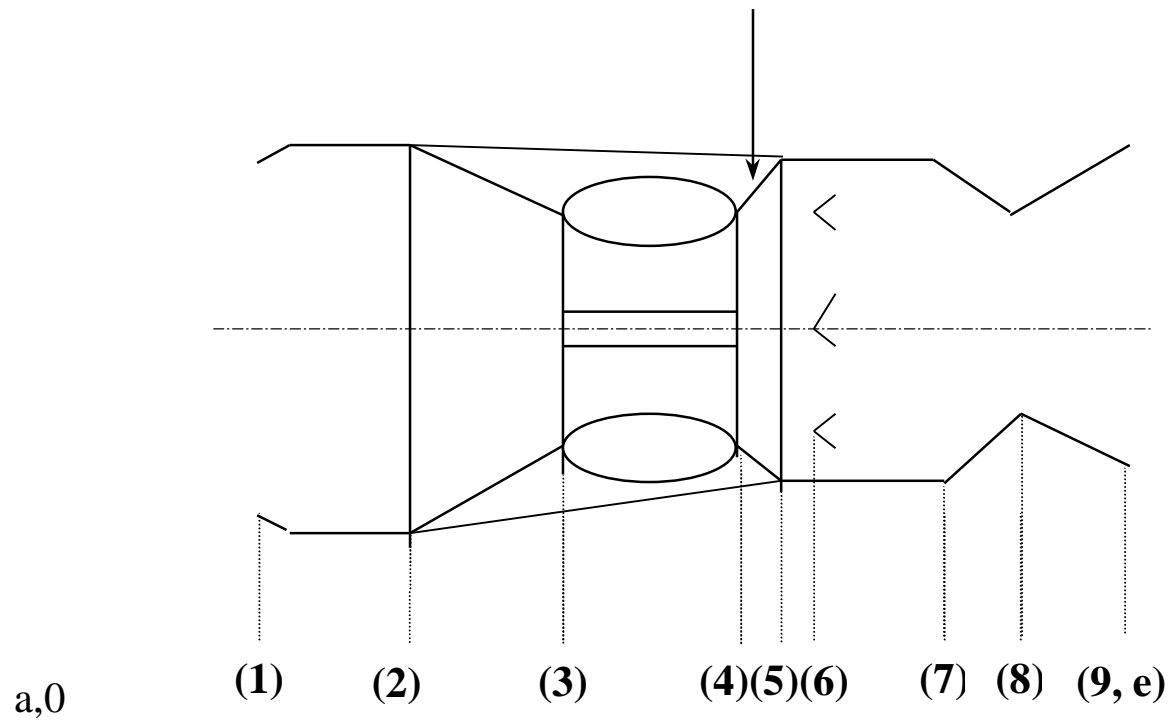
4.3. SIMULINK Program

DYNJET-D4:

4.4. Simulations of the Single-Spool

Engine Control

ENGINE STATIONS



MATHEMATICAL MODEL OF SINGLE-SPOOL ENGINE

$$\dot{m}_{2,corr} = \frac{\dot{m}_{a,c} \sqrt{\frac{T_{02}}{T_{ref}}}}{\frac{P_{02}}{P_{ref}}}$$

$$N_{2,corr} = \frac{N}{\sqrt{\frac{T_{02}}{T_{ref}}}}$$

$$\dot{m}_{4,corr} = \frac{\dot{m}_g \cdot \sqrt{T_{04}}}{P_{04}}$$

$$N_{4,corr} = \frac{N}{\sqrt{T_{04}}}$$

Aircraft Intake (0:1) and Engine Intake (1:2):

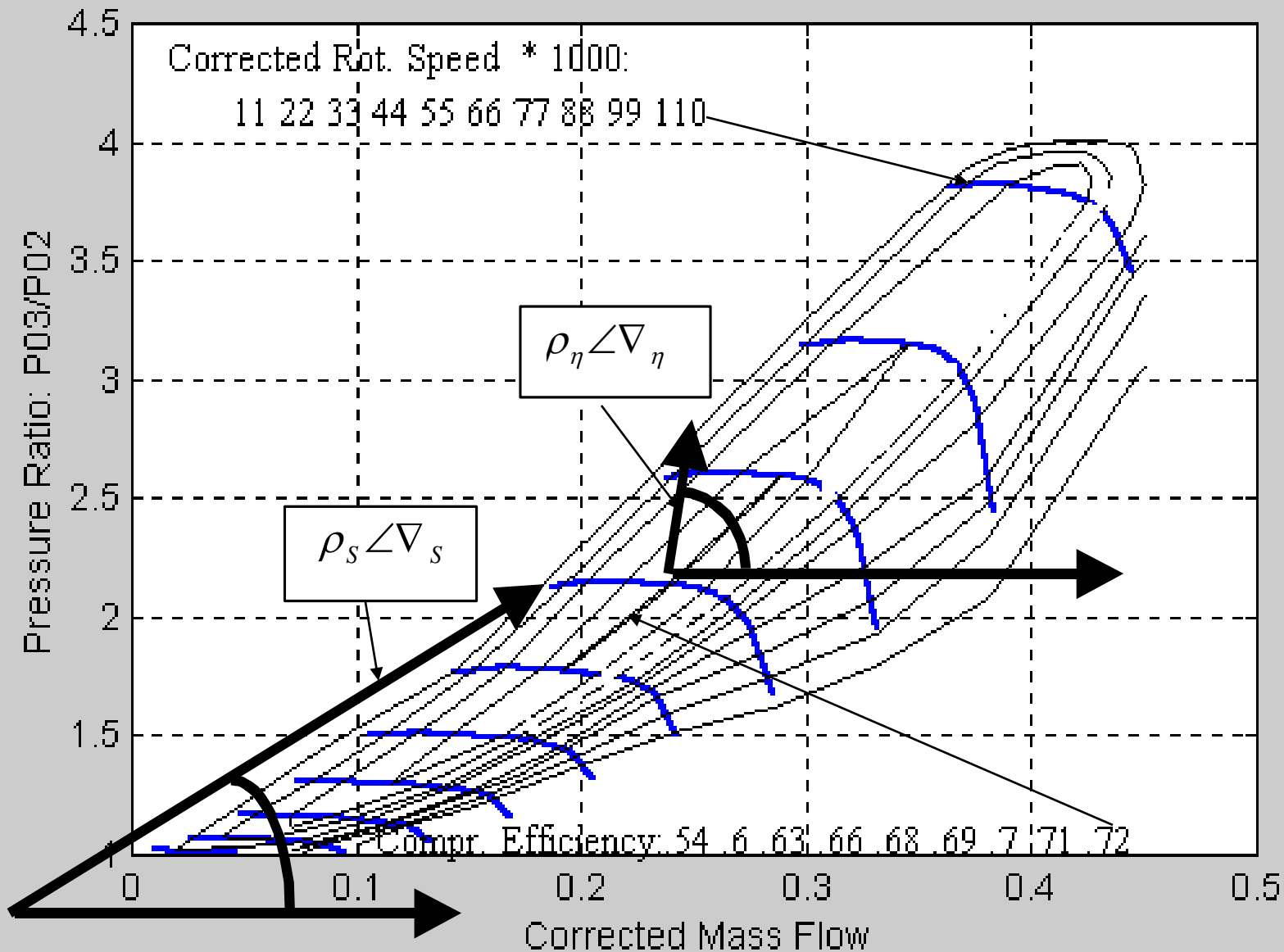
$$\left(\frac{P_{02}}{P_a}\right) = \left[1 + \eta_d \frac{\gamma_a - 1}{2} M^2\right]^{\frac{\gamma_a}{\gamma_a - 1}}$$

$$\left(\frac{T_{02}}{T_a}\right) = 1 + \frac{\gamma_a - 1}{2} M^2$$

Compressor:

$$\left(\frac{P_{03}}{P_{02}} \right) \text{ vs. } \dot{m}_{2,\text{corr}}; \quad N_{2,\text{corr}} - \textit{parameter}$$

$$\left(\frac{P_{03}}{P_{02}} \right) \text{ vs. } \dot{m}_{2,\text{corr}}; \quad \eta_c - \textit{parameter}$$



The Polar Coordinates for Compressor Map Description

Combustor:

$$\left(\frac{P_{04}}{P_{03}} \right) ; \text{ for example: } \left(\frac{P_{04}}{P_{03}} \right) = 0.97$$

$$\eta_b ; \text{ for example: } \eta_b = 0.97$$

Turbine:

$$\dot{m}_{4,\text{corr}} \text{ vs. } \left(\frac{P_{04}}{P_{05}} \right), \quad N_{4,\text{corr}} = \text{parameter}$$

$$\eta_t \text{ vs. } \left(\frac{P_{04}}{P_{05}} \right), \quad N_{4,\text{corr}} = \text{parameter}$$

Exhaust Diffuser and Jet Pipe:

$$\frac{P_{05} - P_{07}}{P_{05}}$$

for example: $\frac{P_{05} - P_{07}}{P_{05}} = 0.020$;

Nozzle:

$$\dot{m}_{7,\text{corr}} = \dot{m}_{7,\text{corr, theor}} \cdot C_D$$

$$\dot{m}_{7,\text{corr,theor}} = \sqrt{2 \cdot \eta_n \cdot C_p \cdot \left[1 - \left(\frac{1}{\left(\frac{P_{07}}{P_a} \right)^{\frac{\gamma_g - 1}{\gamma_g}}} \right) \right]} \cdot \frac{A_e}{R} \cdot \frac{1}{\left(\frac{P_{07}}{P_a} \right)} \cdot \frac{1}{1 - \eta_n \left[1 - \left(\frac{1}{\left(\frac{P_{07}}{P_a} \right)^{\frac{\gamma_g - 1}{\gamma_g}}} \right) \right]}$$

Fuel Pump:

$$\tau_f \cdot \frac{d\dot{m}_f}{dt} + \dot{m}_f = (0.0098 \cdot V_f^2 + 0.5095V_f + 0.8868) \cdot 10^{-3}, \left[\frac{kg}{s} \right]$$

$$\tau_f = \frac{0.2}{1 + 0.204 \cdot V_f}$$

Alternator:

Alternator power;

for example altpower = 0... 800, [Watt]

The Engine Equations:

$$f = C_{p_{gt}} \cdot (T_{04} - T_{03}) / Q_R \cdot \eta_b - C_{p_{gt}} \cdot T_{04}$$

$$\dot{m}_g = \dot{m}_a + \dot{m}_f$$

$$C_{p_{gt}} \cdot \dot{m}_g \cdot (T_{04} - T_{05}) \cdot \eta_m - C_{p_{ac}} \cdot \dot{m}_a \cdot (T_{03} - T_{02}) - \text{altpower} = \frac{dE}{dt}$$

$$E = \frac{J \cdot N^2 \cdot \pi^2}{1800}$$

$$\text{For } \frac{P_{07}}{P_a} < \frac{P_{07}}{P_{cr}}$$

$$u_e = \sqrt{2\eta_n \cdot C_p \cdot T_{07} \cdot \left(1 - \frac{P_a}{P_{07}}\right)^{\frac{\gamma_g - 1}{\gamma_g}}}$$

$$T = \dot{m}_a \cdot [C_x(1+f)u_e - u_a \cdot (1+\varepsilon)]$$

For

$$\frac{P_{07}}{P_a} \geq \frac{P_{07}}{P_{cr}}$$

$$u_e = \sqrt{2 \cdot \eta_n \cdot C_{p_{gt}} \cdot T_{07} \cdot \left(1 - \left(\frac{P_{cr}}{P_{07}} \right)^{\frac{\gamma_g - 1}{\gamma_g}} \right)}$$

$$T = \dot{m}_a [C_x (1 + f) u_e - u_a \cdot (1 + \varepsilon)] + (P_{cr} - P_a) \cdot A$$

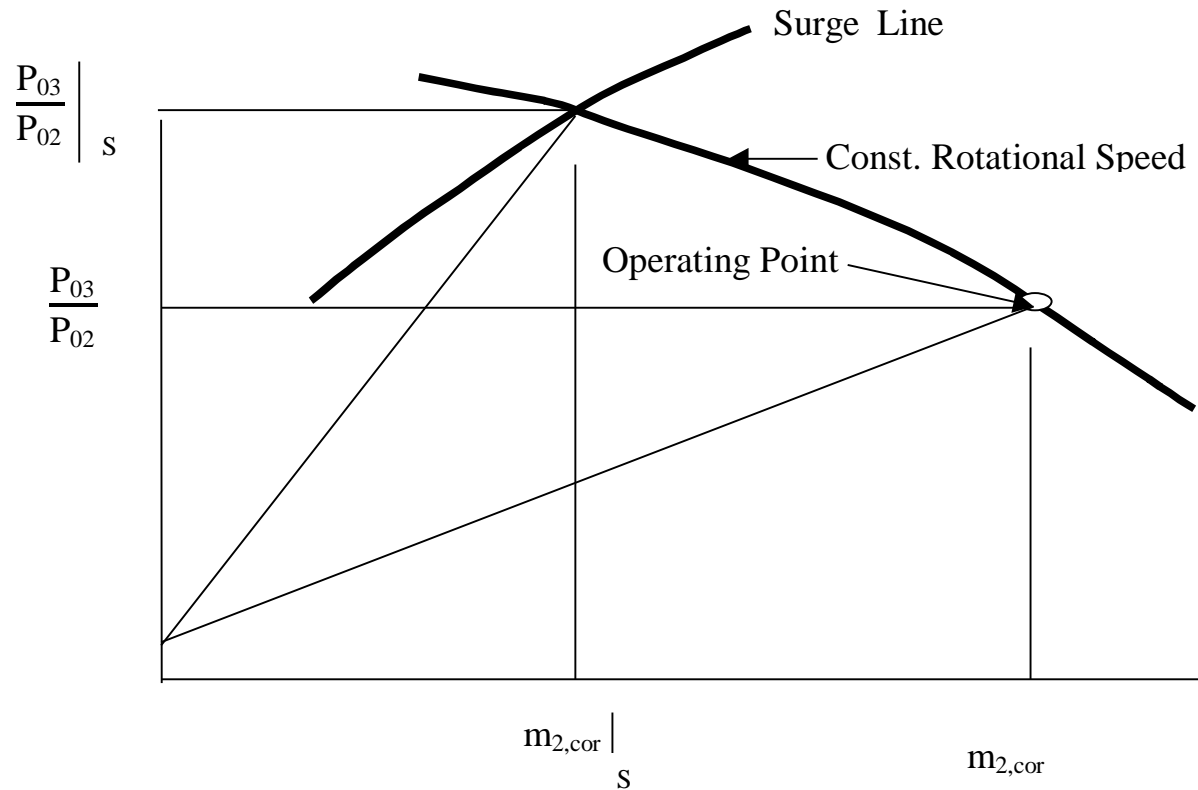
$$SFC = \frac{f \cdot \dot{m}_a}{T}$$

Equivalence Ratio:

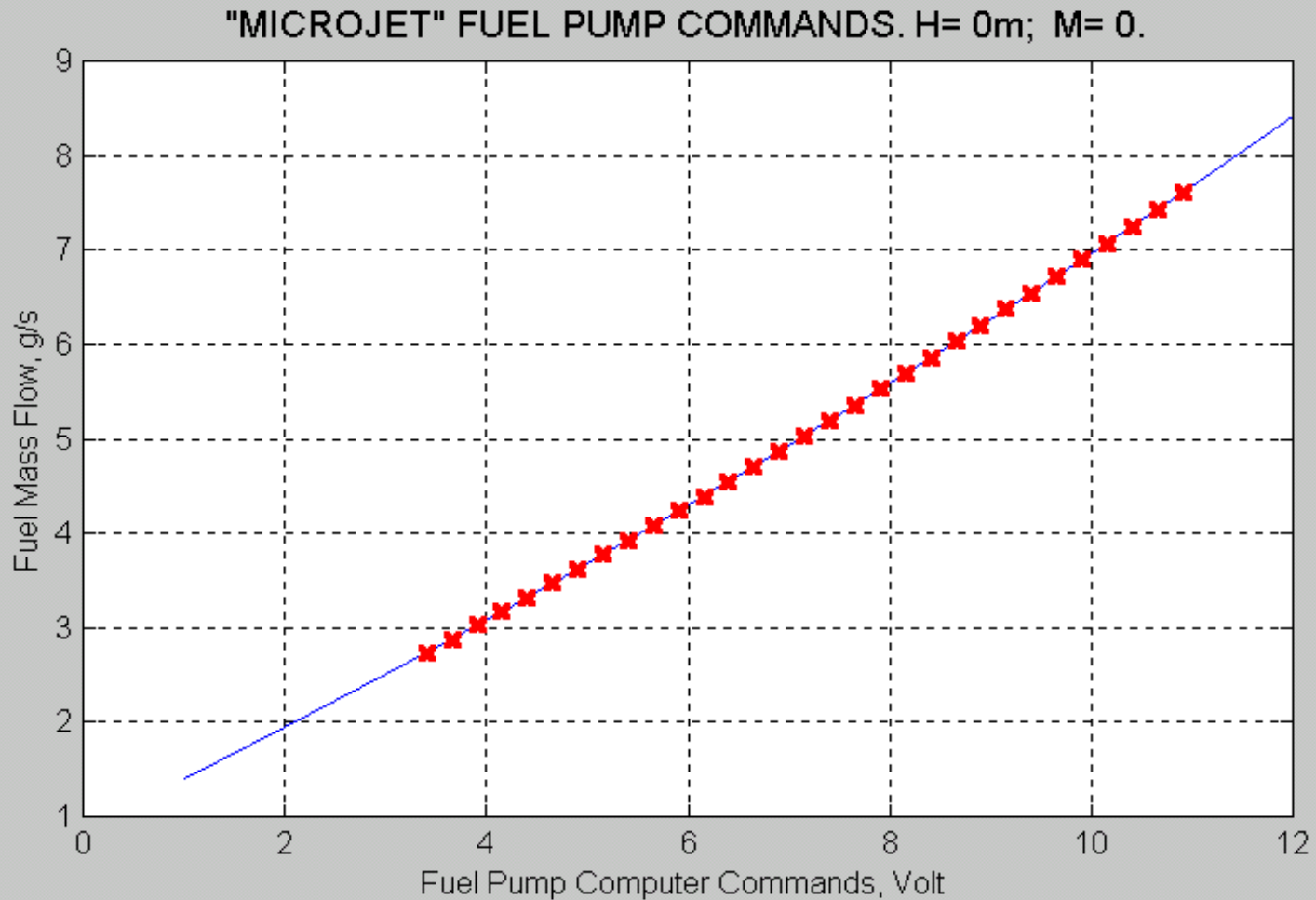
$$\phi = \frac{\frac{\dot{m}_f}{\dot{m}_a}}{\frac{\dot{m}_f}{m_a} \Big|_{stoch}}$$

Stall Margin Definition

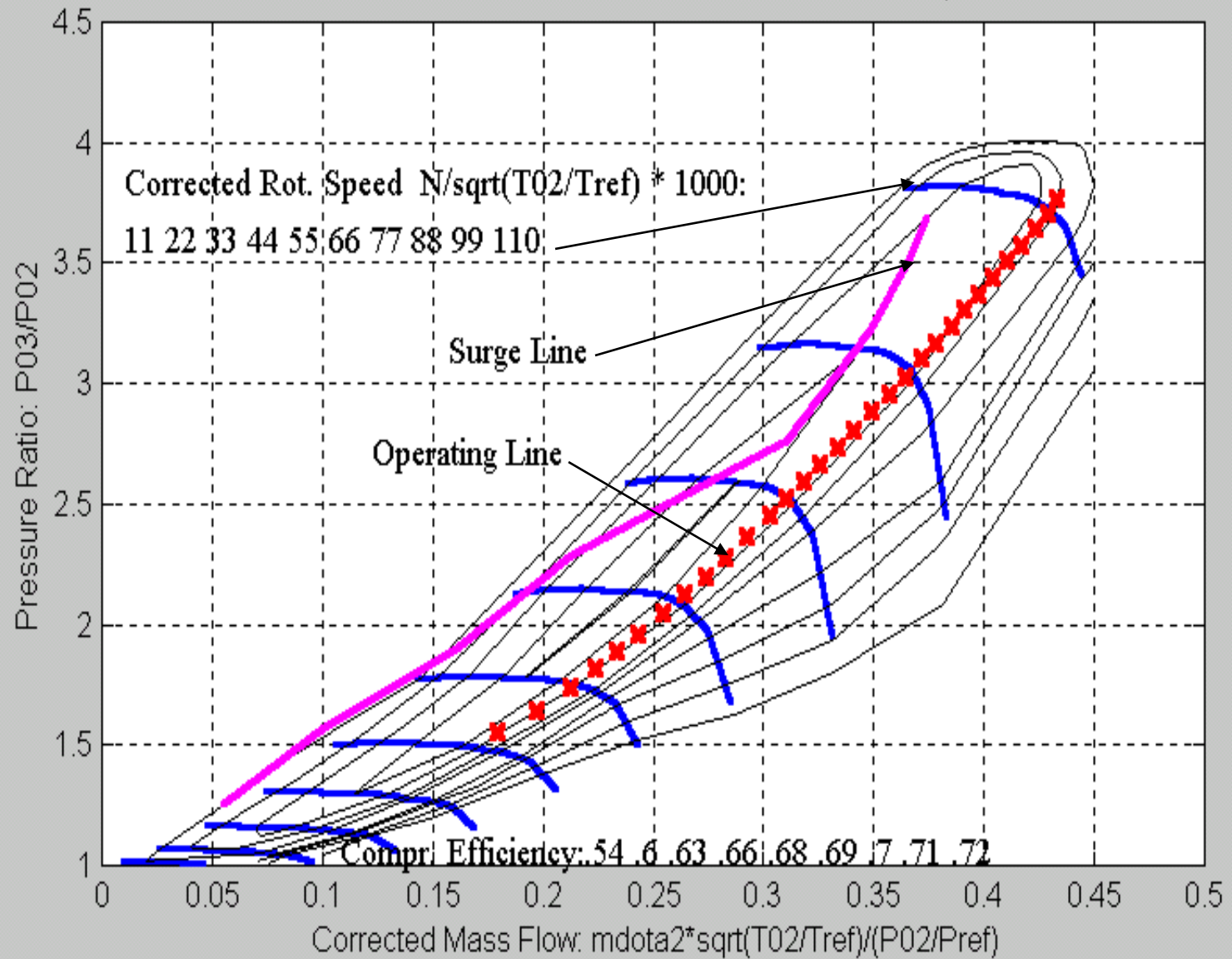
$$SM = \frac{\left(\frac{P_{03}}{P_{02}} \right)_s}{\left(\dot{m}_{2,cor} \right)_s} - \frac{\frac{P_{03}}{P_{02}}}{\dot{m}_{2,cor}}$$



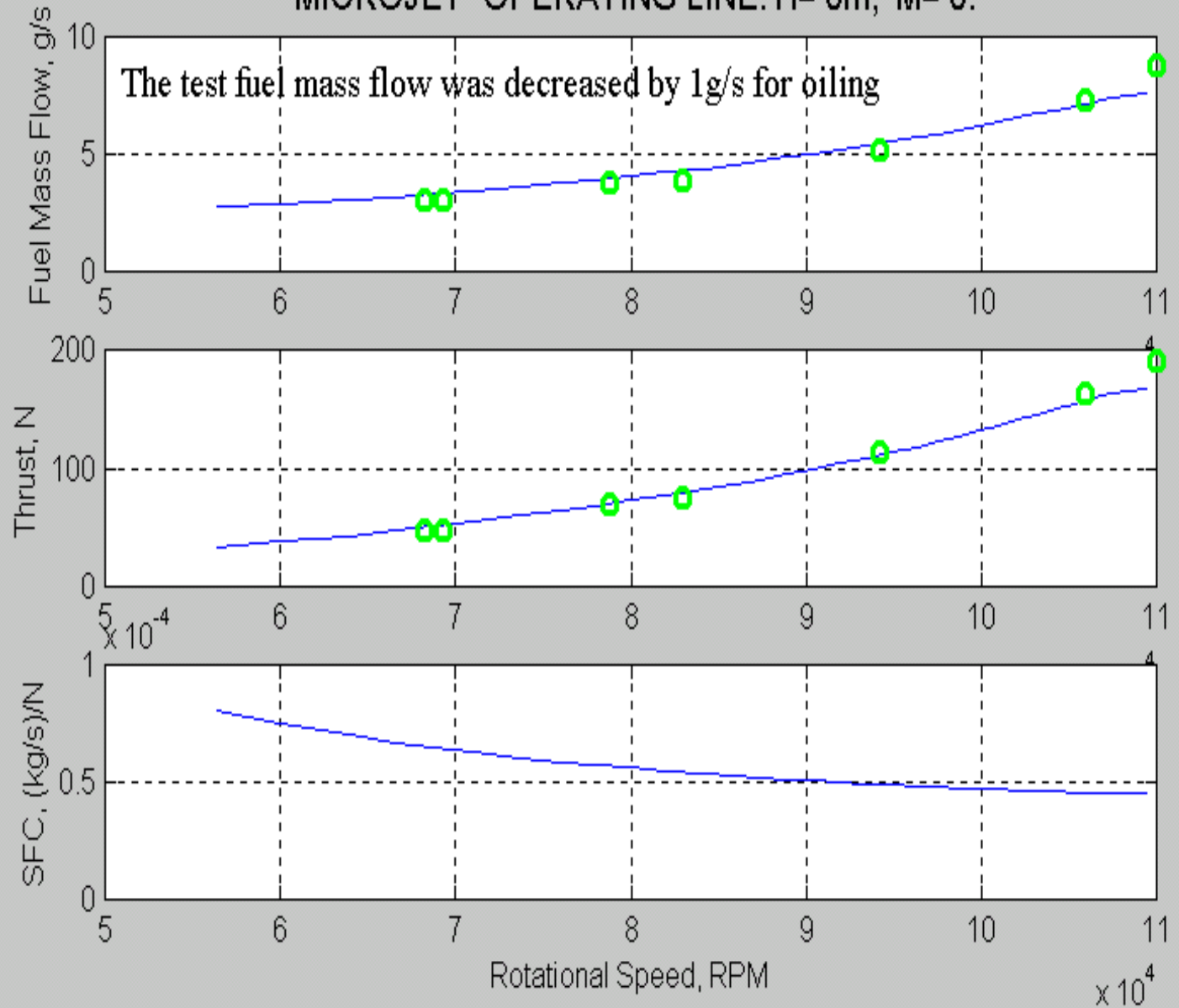
“MICROJET” OPEN LOOP STEADY-STATE SIMULATIONS in MATLAB



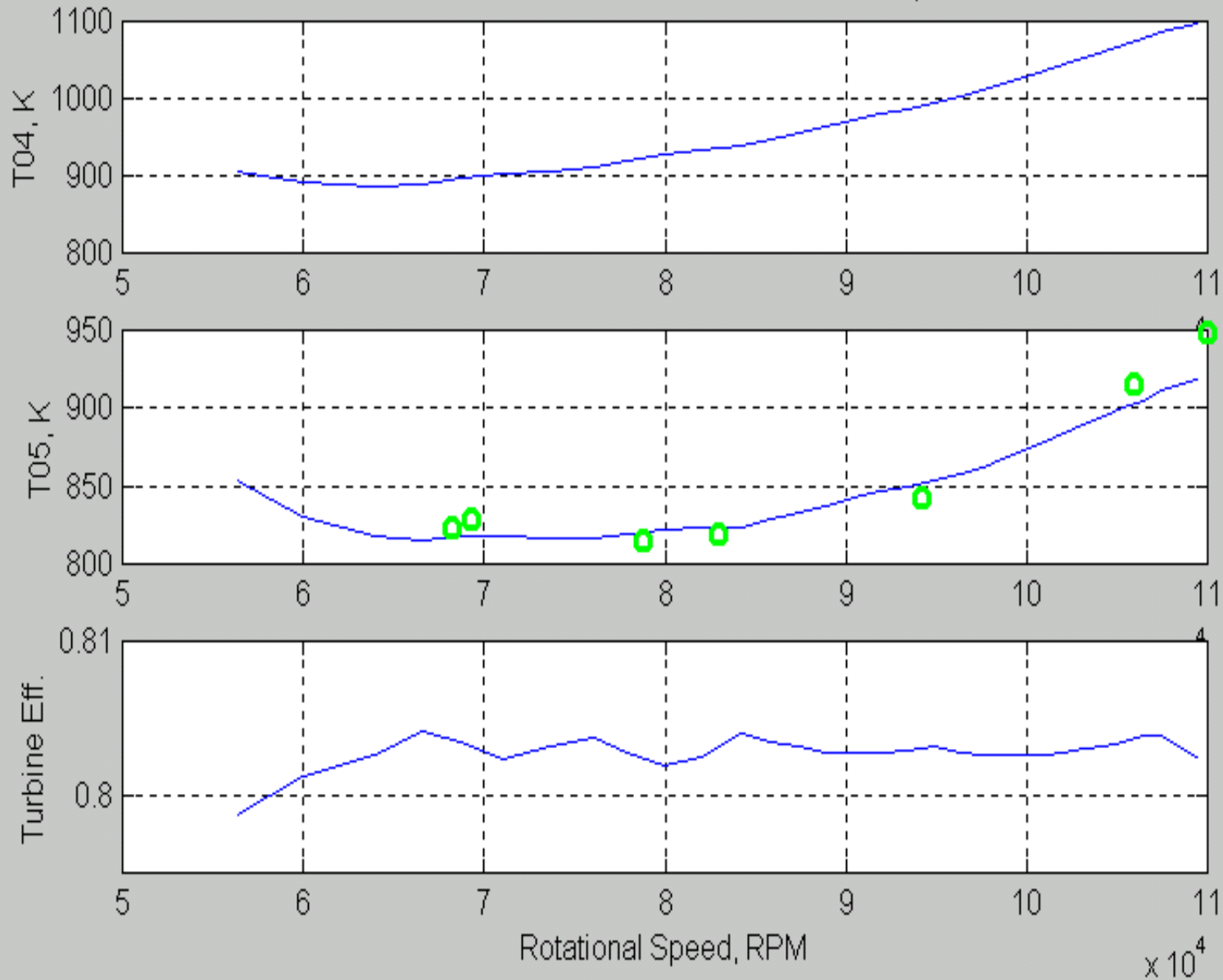
"MICROJET" COMPRESSOR MAP. H= 0m; M= 0.



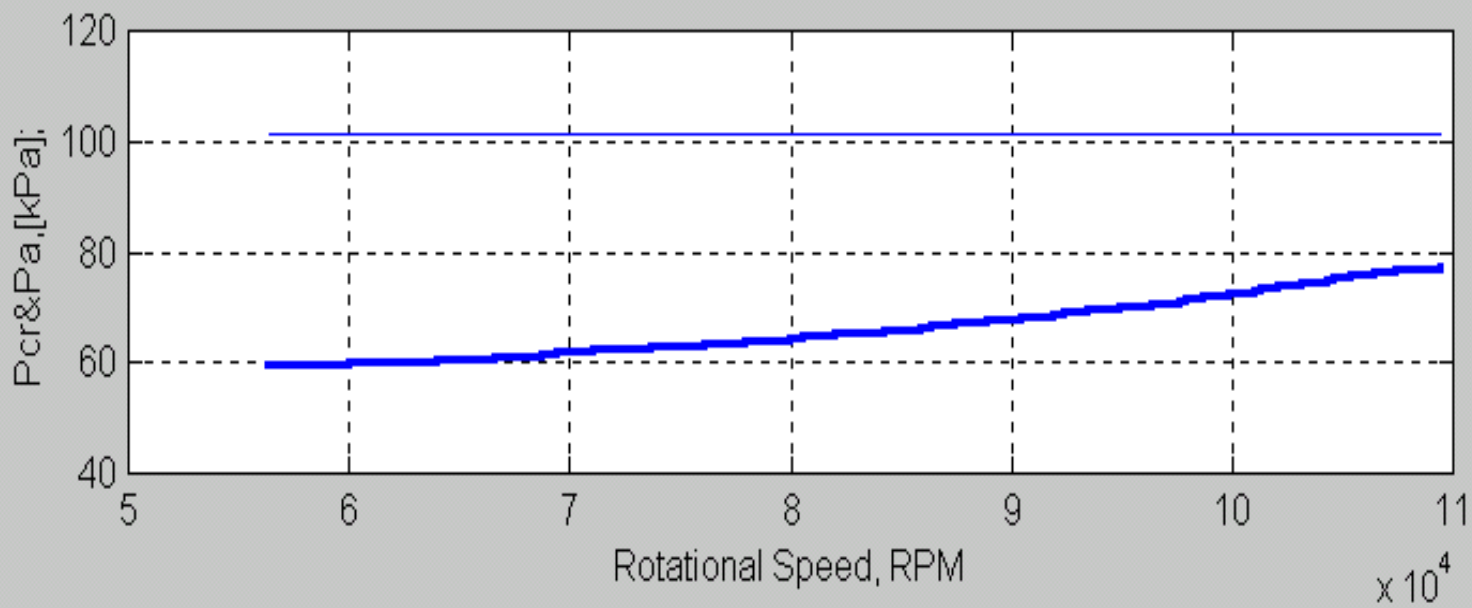
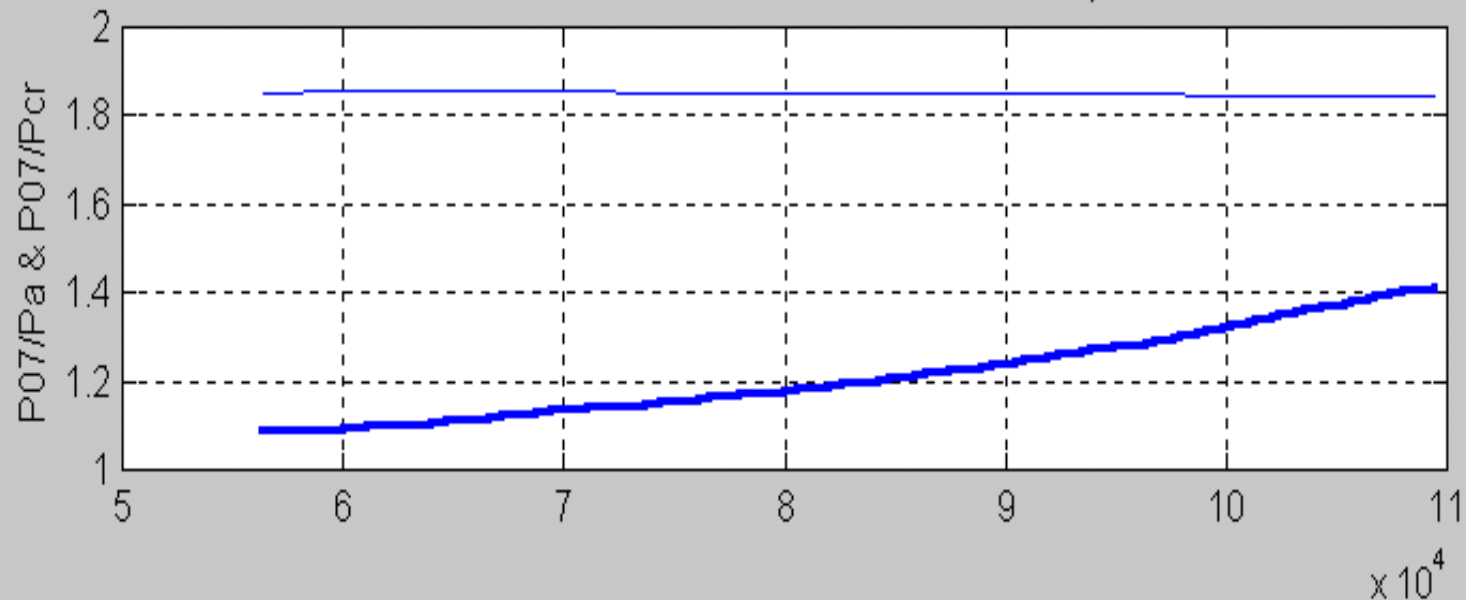
"MICROJET" OPERATING LINE. H= 0m; M= 0.



"MICROJET" OPERATING LINE. H= 0m; M= 0.



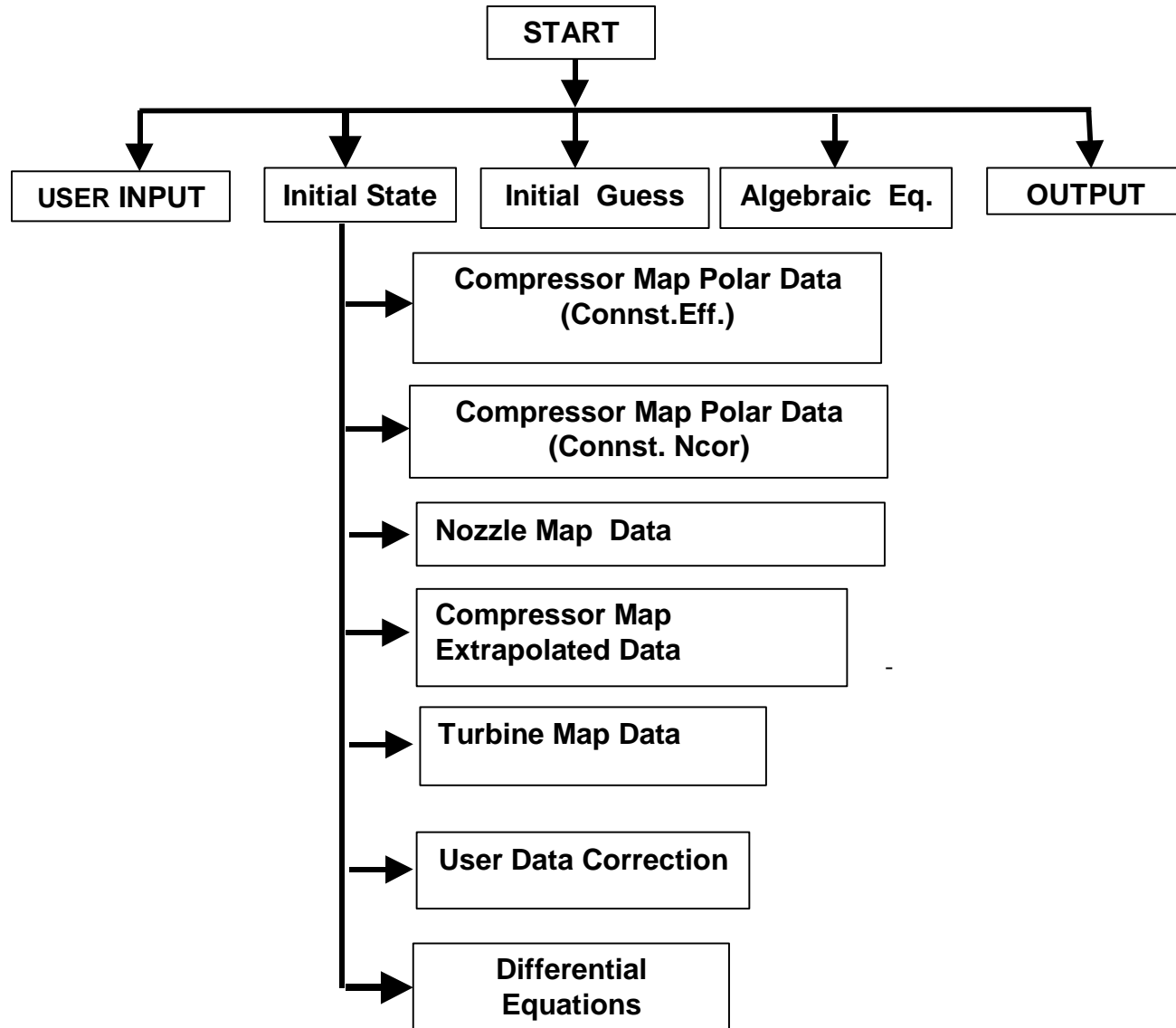
"MICROJET" OPERATING LINE. H= 0m; M= 0.



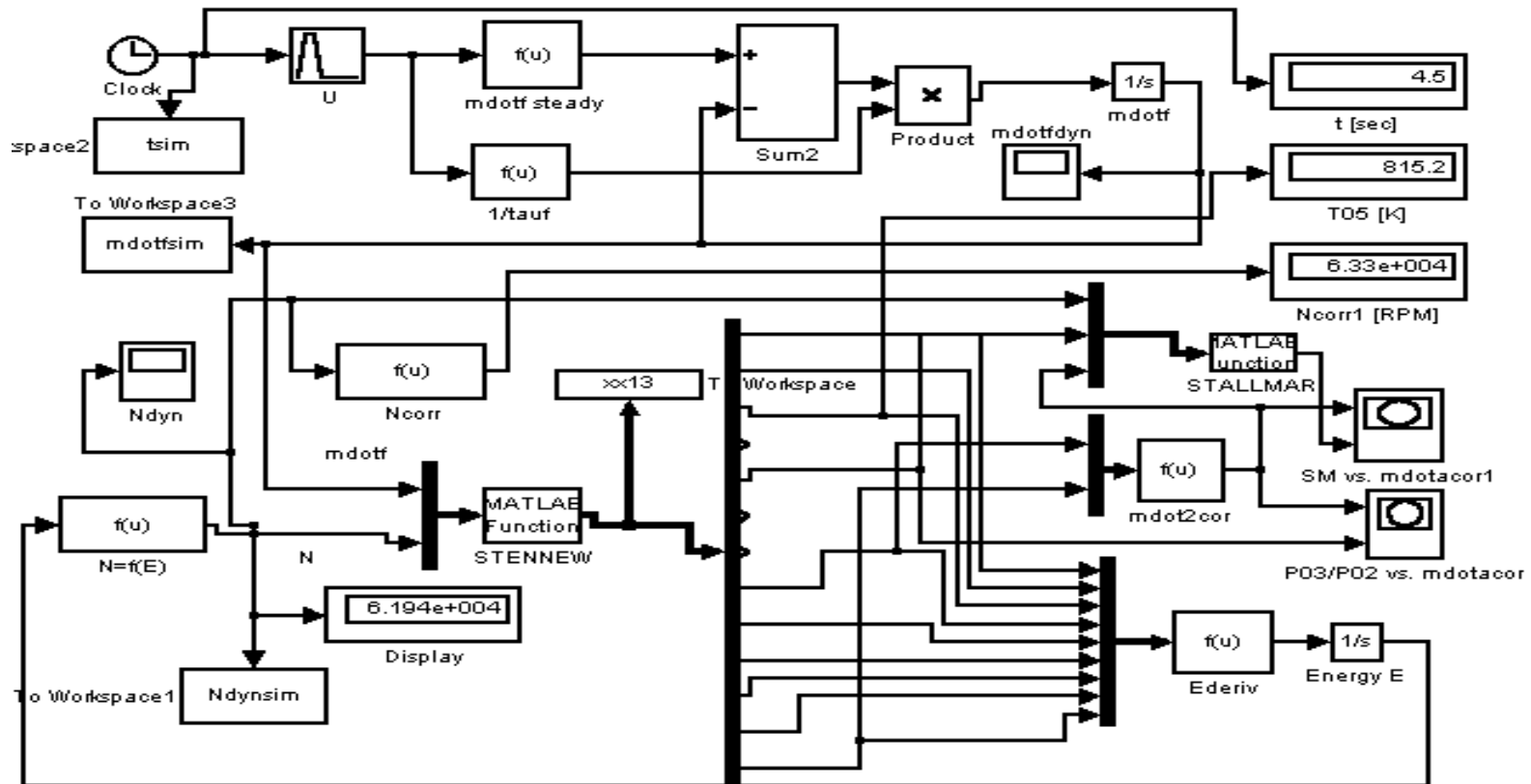
Dynamic Model Input Parameters

No.	Parameter	Notation
1.	Mach Number	M
2.	Altitude	H, [ft]
3.	Commands: - time vector - fuel pump voltage vector	t, [s] V, [Volt]
4.	Alternator electrical power	W, [Watt]
5.	Stall margin limit	<i>SM</i> _{lim}
6.	Equivalence ratio: - minimum - maximum	ϕ _{min} ϕ _{max}
7.	Turbine inlet temperature limit	T_{04max} [K]

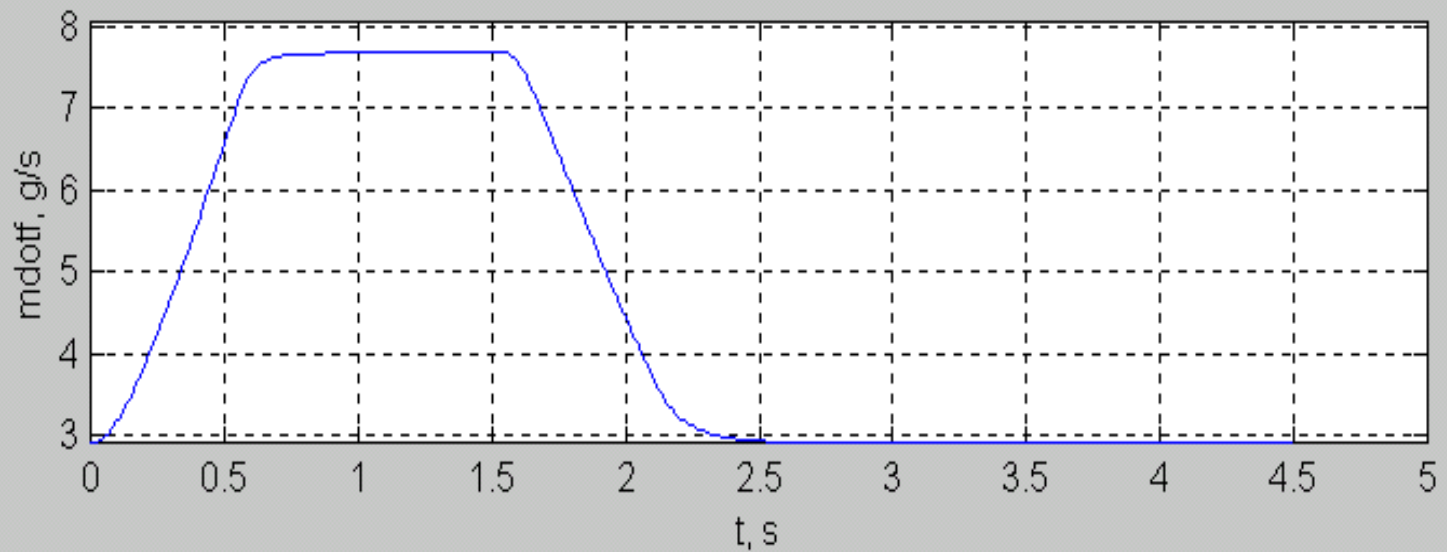
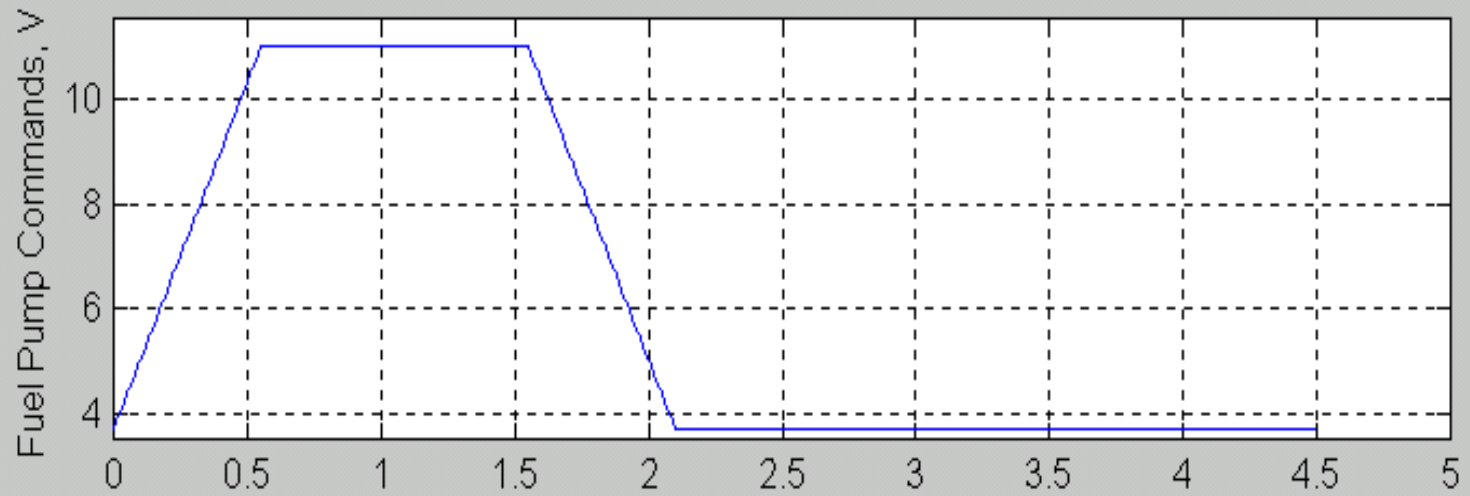
DYNJET-2 BLOCK-DIAGRAM



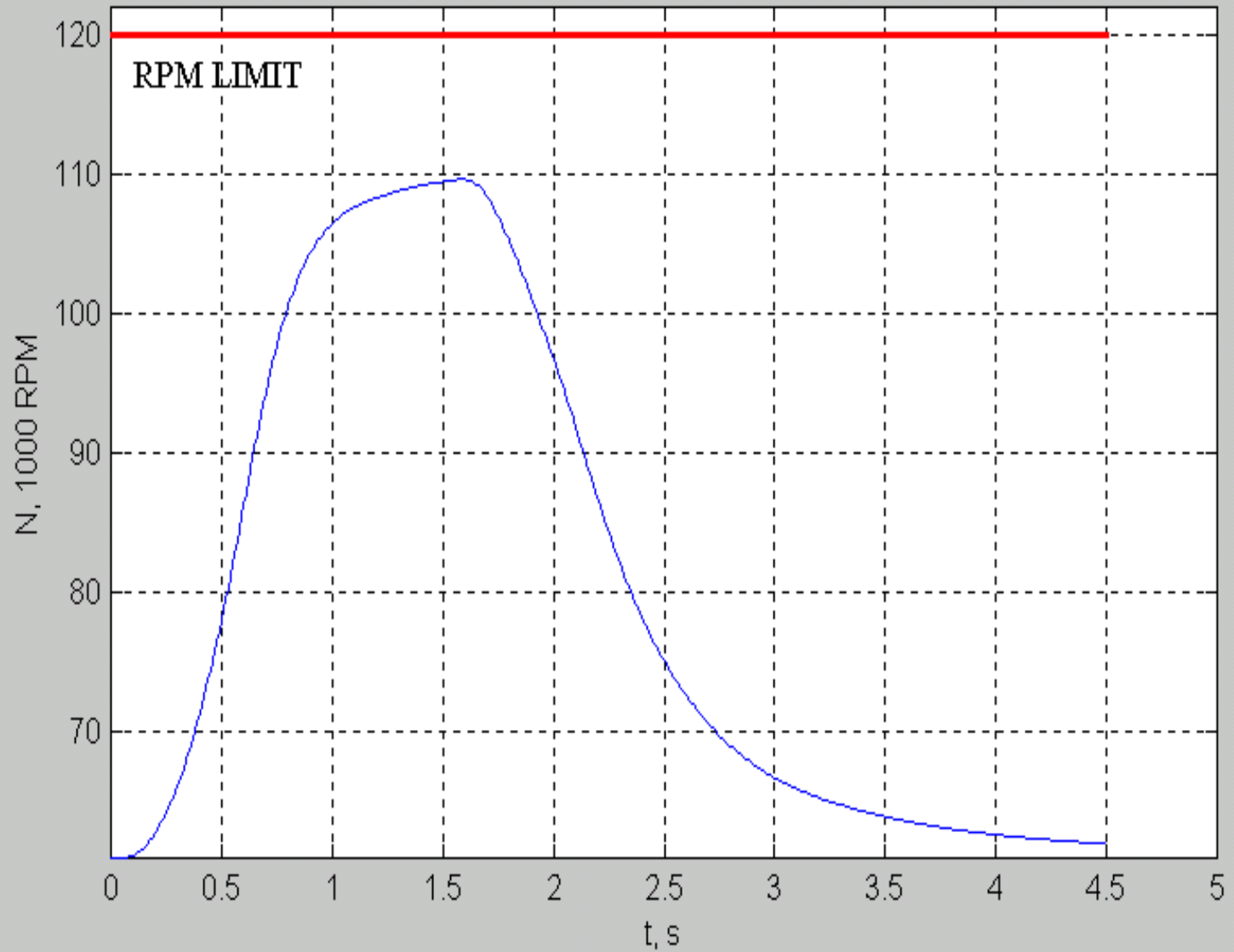
SIMULINK PROGRAM FOR "MICROJET" OPEN-LOOP SIMULATIONS



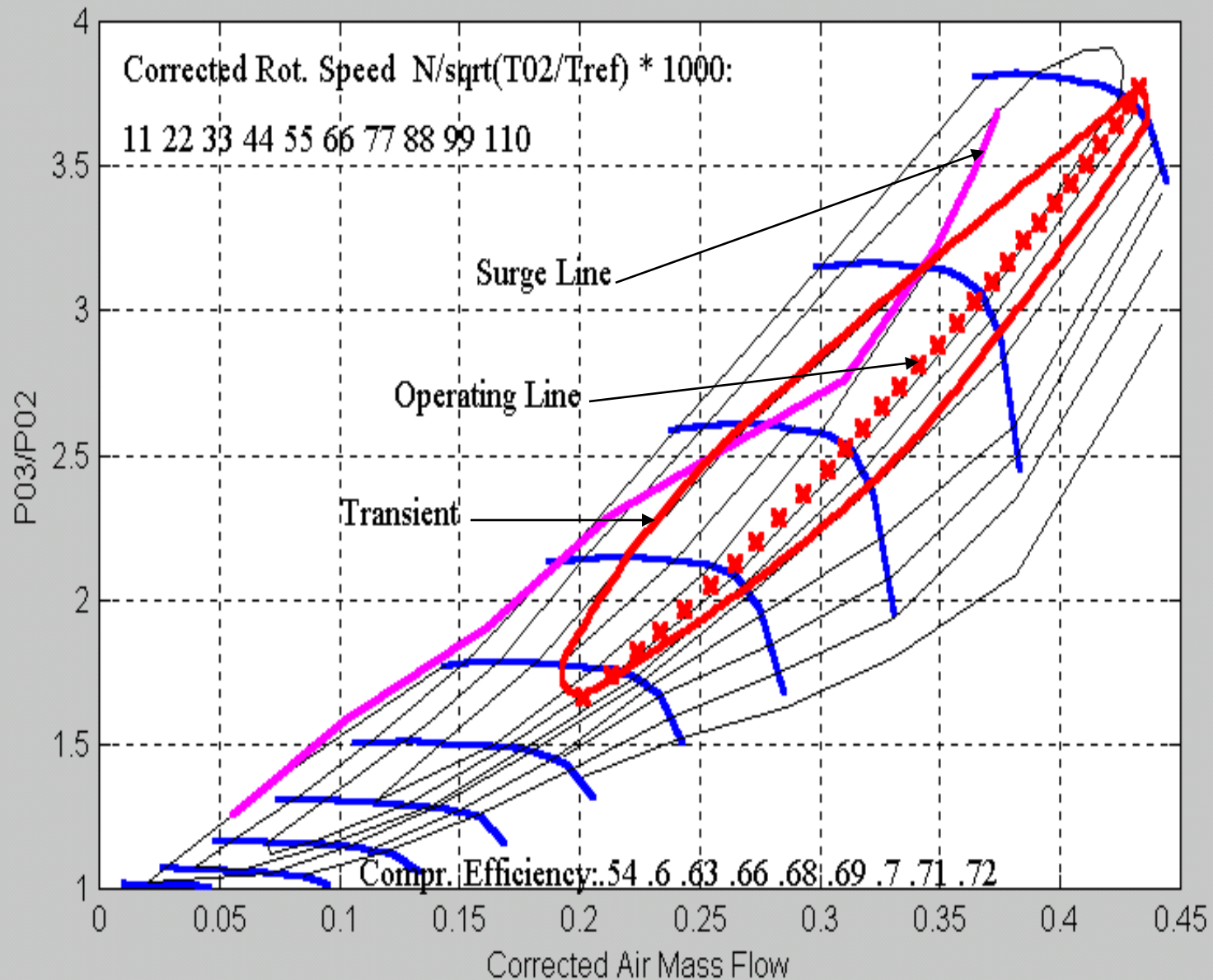
"MICROJET" OPEN-LOOP TRANSIENT. H= 0m; M= 0.



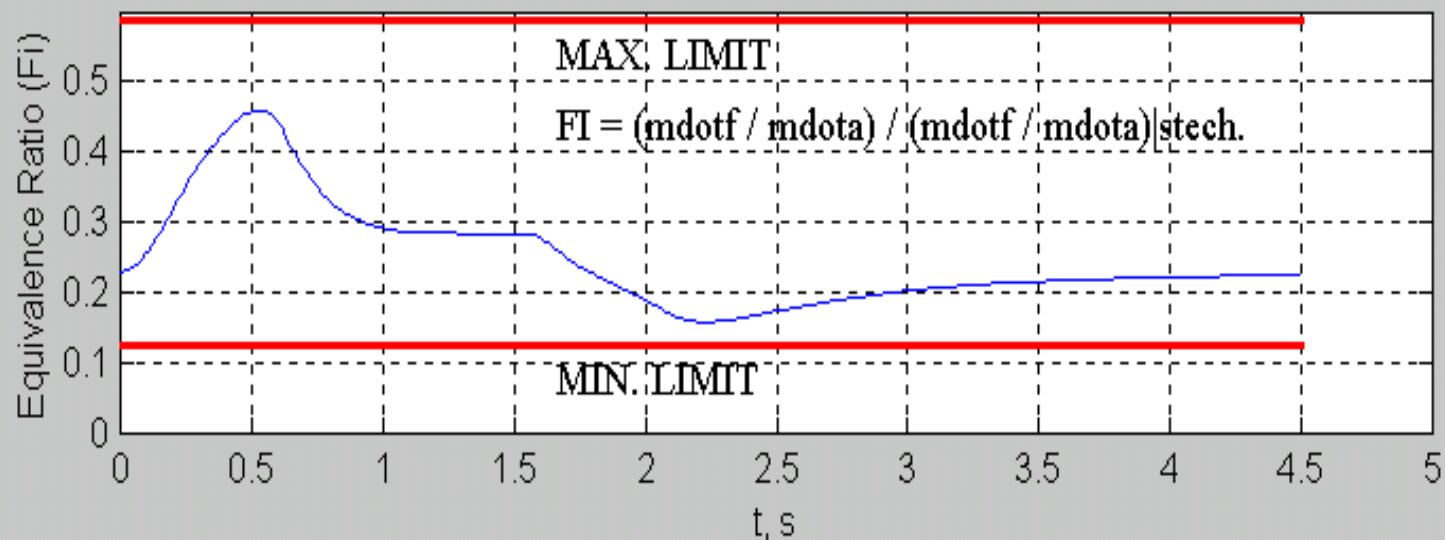
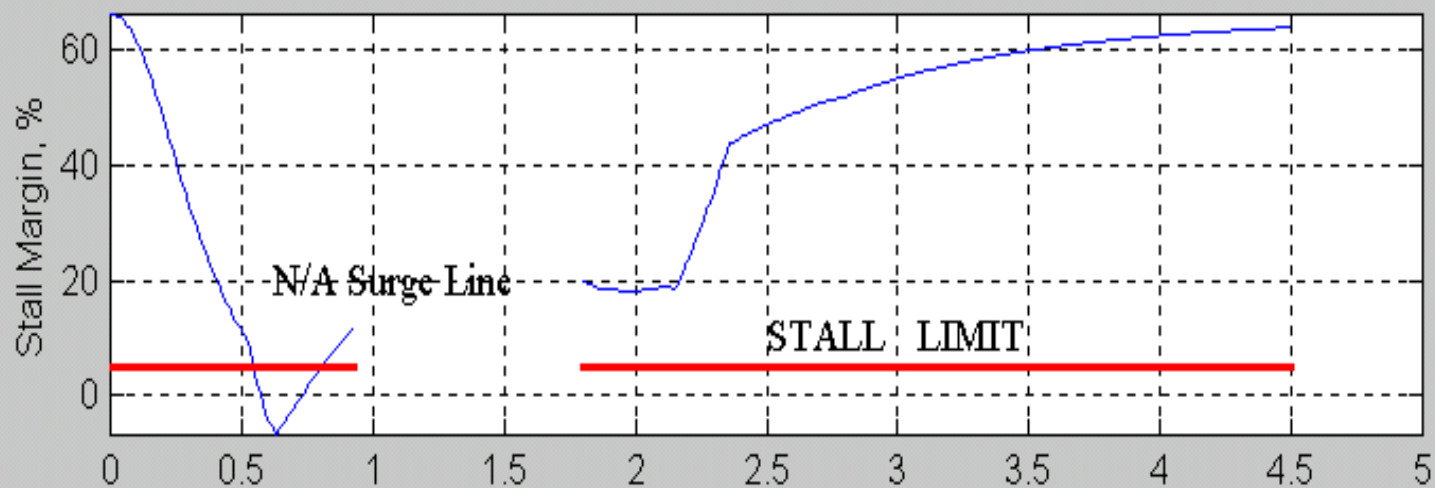
"MICROJET" OPEN-LOOP TRANSIENT. H= 0m; M= 0.



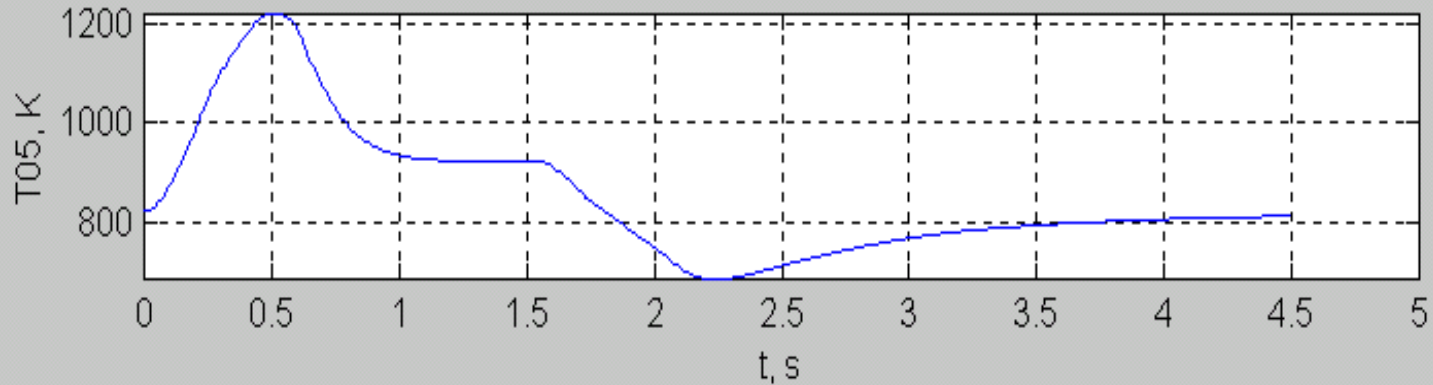
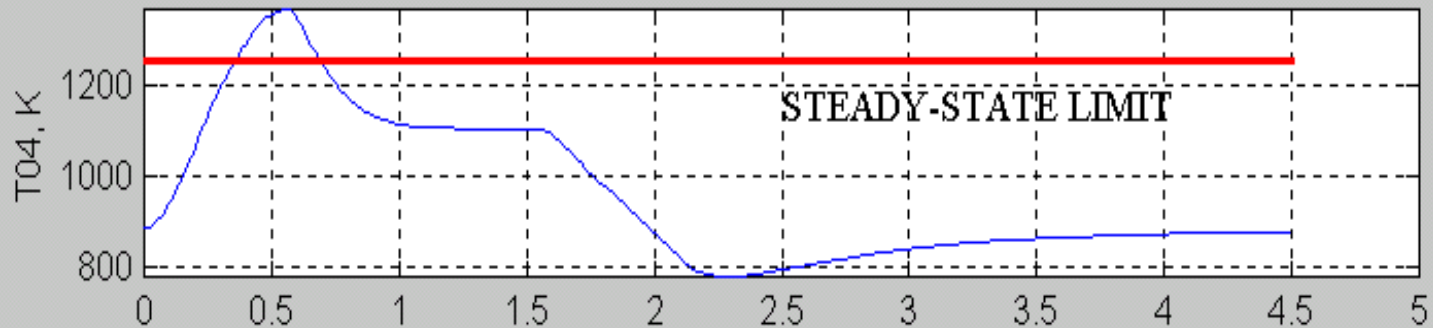
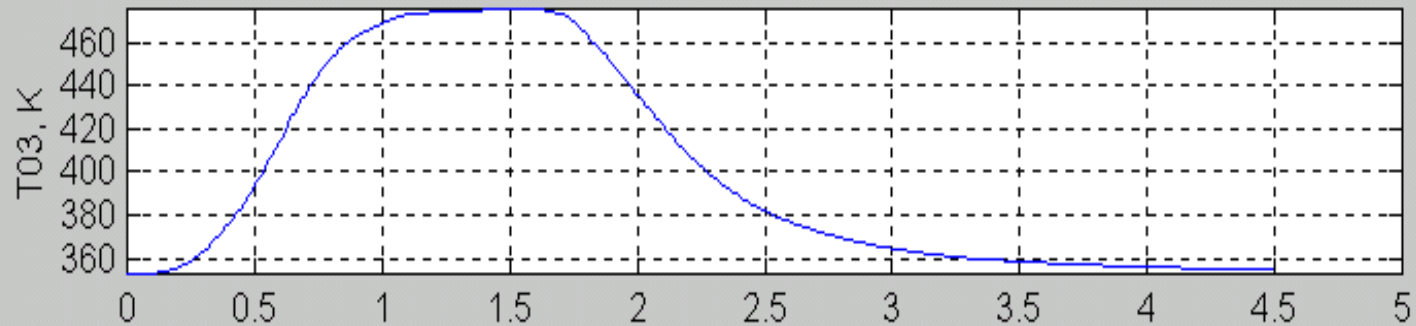
"MICROJET" OPEN-LOOP TRANSIENT. H= 0m; M= 0.



"MICROJET" OPEN-LOOP TRANSIENT. H= 0m; M= 0.



"MICROJET" OPEN-LOOP TRANSIENT. H= 0m; M= 0.



CONTROL PROBLEM:

1. Corrected rotational speed (N_{cor}) control:

a) Steady-state error: $<1\%$

b) Settling time: minimum

c) Overshoot: $<2\%$

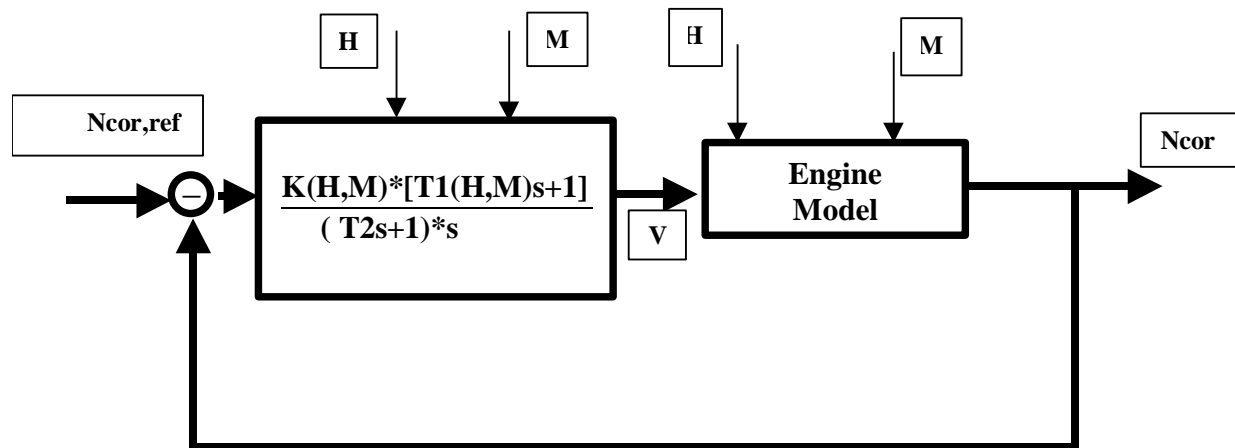
2. Stall margin: $>5\%$

3. T_{05} : $<T_{05max}$

4. Equivalence Ratio: $\phi_{min} < \phi < \phi_{max}$

Engine Control System

Flight Conditions: $0 < H < 20,000\text{ft}$ and $0 < M < 0.7$



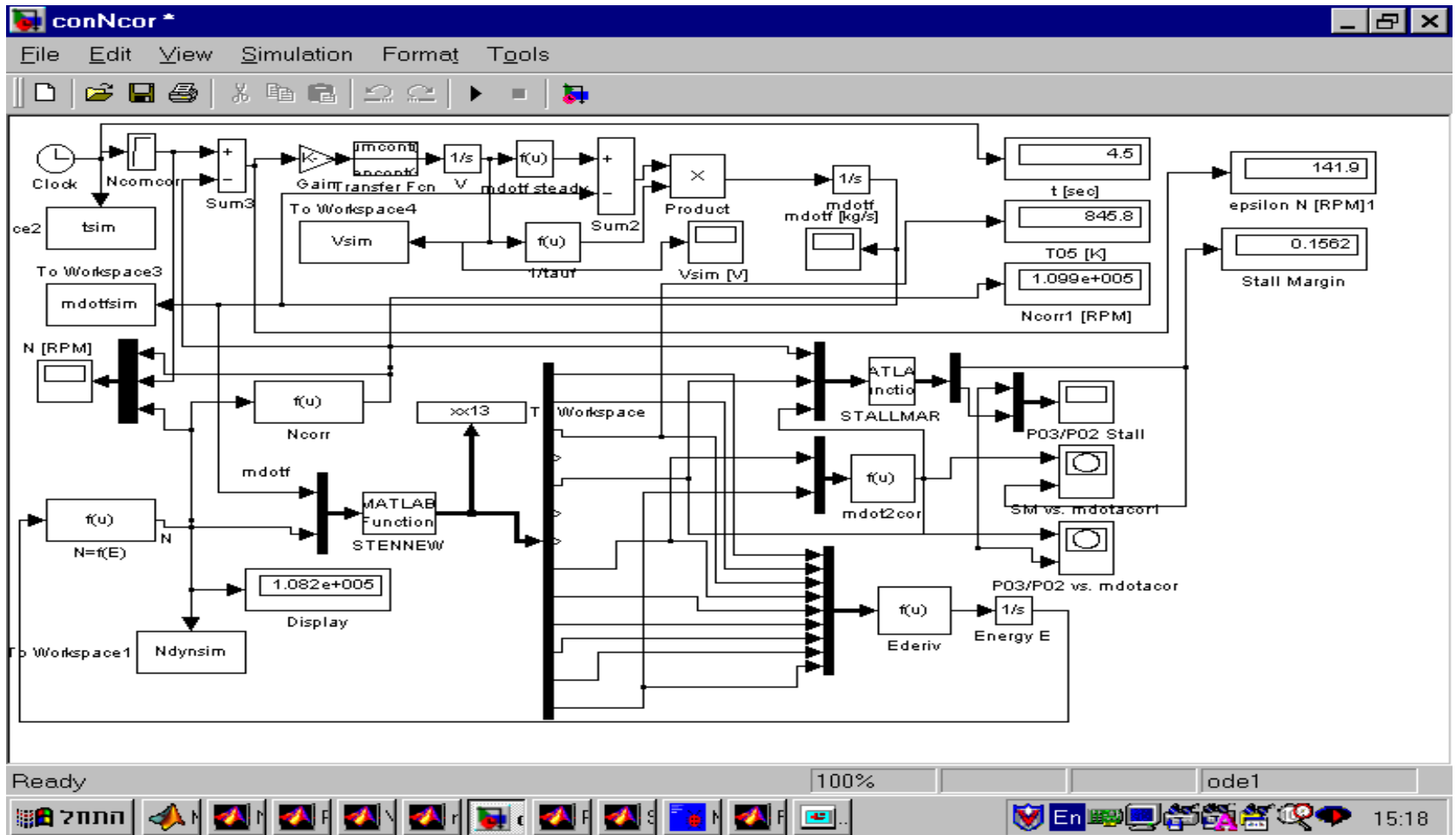
NONLINEAR CONTROLLER – T1 [s]:

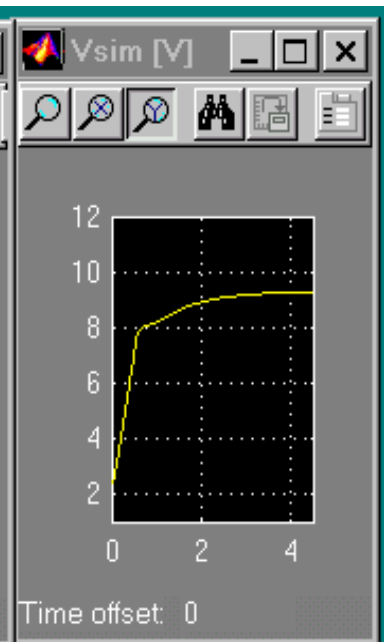
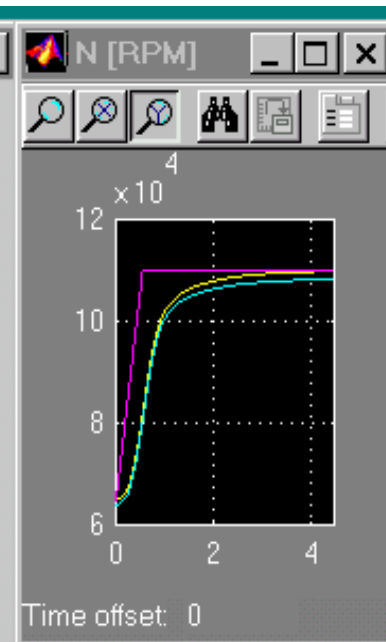
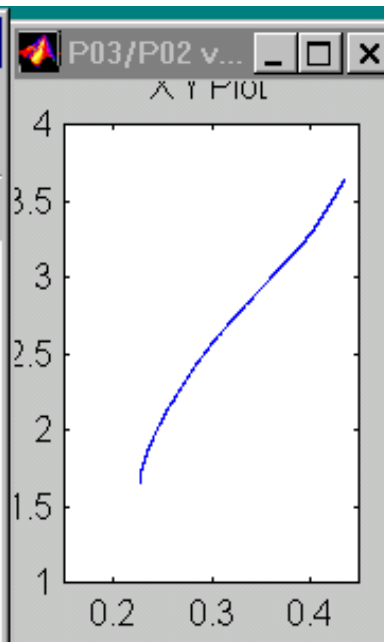
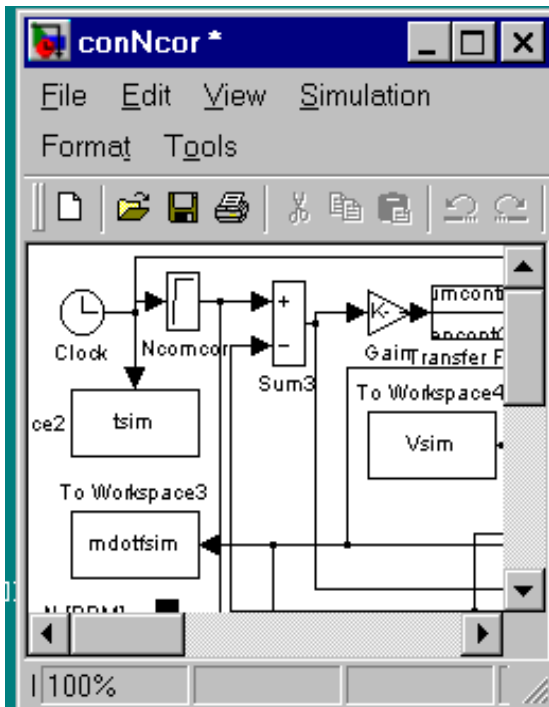
Hfeet / M	0	0.1	0.25	0.5	0.6	0.7
0	1.00	1.00	1.00	1.00	1.50	2.00
1000	0.70	0.60	0.80	0.80	1.40	1.70
2000	0.60	0.60	0.70	0.75	0.80	1.00
3000	0.40	0.40	0.40	0.40	0.40	0.50
4000	0.20	0.25	0.30	0.30	0.35	0.45
5000	0.20	0.20	0.25	0.30	0.35	0.40
7500	0.20	0.20	0.225	0.30	0.30	0.40
10000	0.20	0.17	0.20	0.30	0.30	0.40
15000	0.17	0.15	0.20	0.30	0.30	0.40
20000	0.15	0.15	0.20	0.30	0.30	0.40

NONLINEAR CONTROLLER – K [V*s/RPM]:

Hfeet / M	0	0.1	0.25	0.5	0.6	0.7
0	0.000100	0.00011	0.00014	0.00025	0.00050	0.00075
1000	0.000100	0.00012	0.00015	0.00025	0.00070	0.00100
2000	0.000075	0.00010	0.00016	0.00030	0.00073	0.00100
3000	0.000075	0.00010	0.00017	0.00035	0.00070	0.00150
4000	0.000075	0.00010	0.00015	0.00035	0.00070	0.00140
5000	0.000075	0.00010	0.00010	0.00030	0.00060	0.00050
7500	0.000075	0.00006	0.00010	0.00025	0.00040	0.00050
10000	0.000050	0.00006	0.00010	0.00020	0.00030	0.00040
15000	0.000030	0.00005	0.00007	0.00015	0.00017	0.00030
20000	0.000020	0.00003	0.00004	0.00010	0.00015	0.00020

SIMULINK PROGRAM FOR “MICROJET” CLOSE-LOOP SIMULATIONS



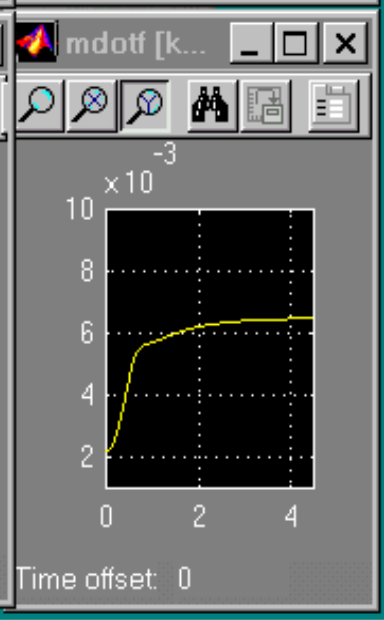
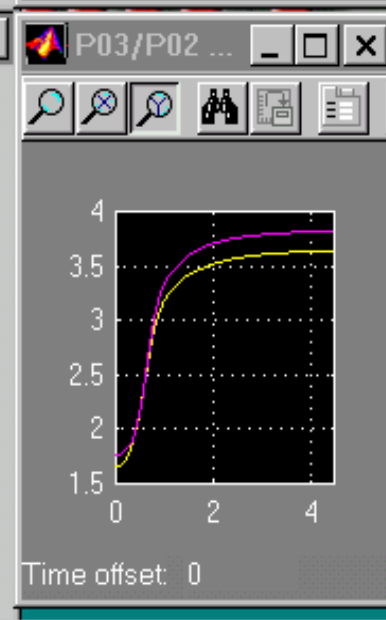
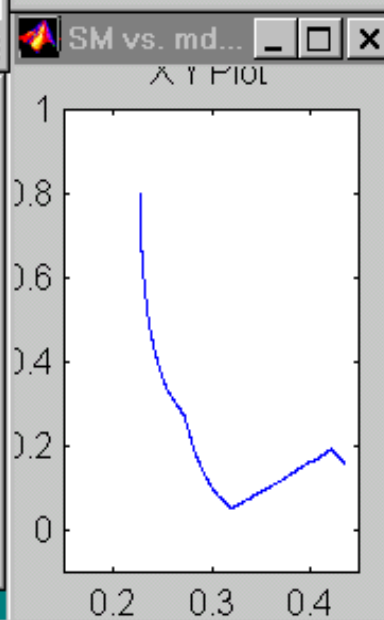


MATLAB Command ...

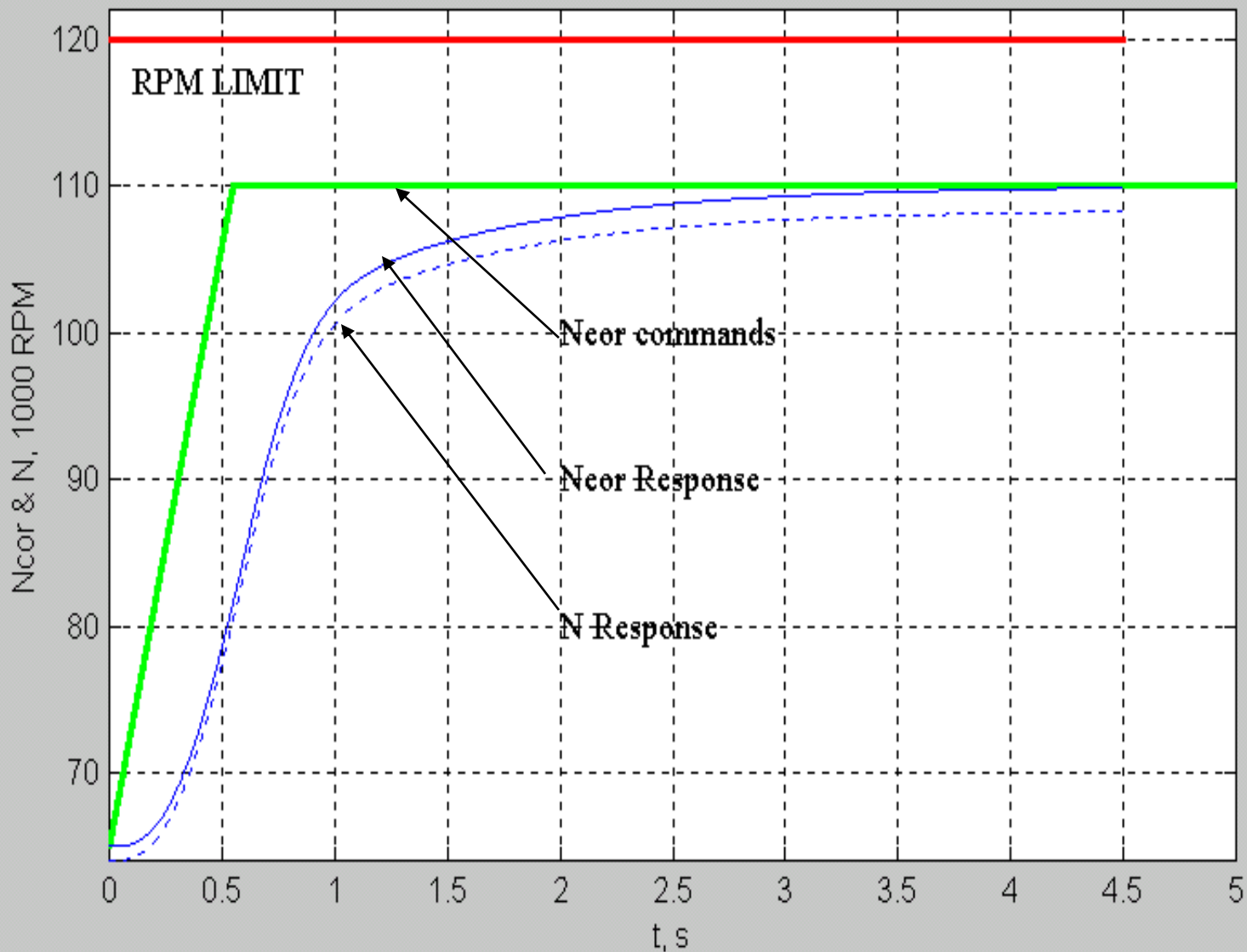
File Edit View Window Help

```
4.49    0.0165
4.50    0.0165
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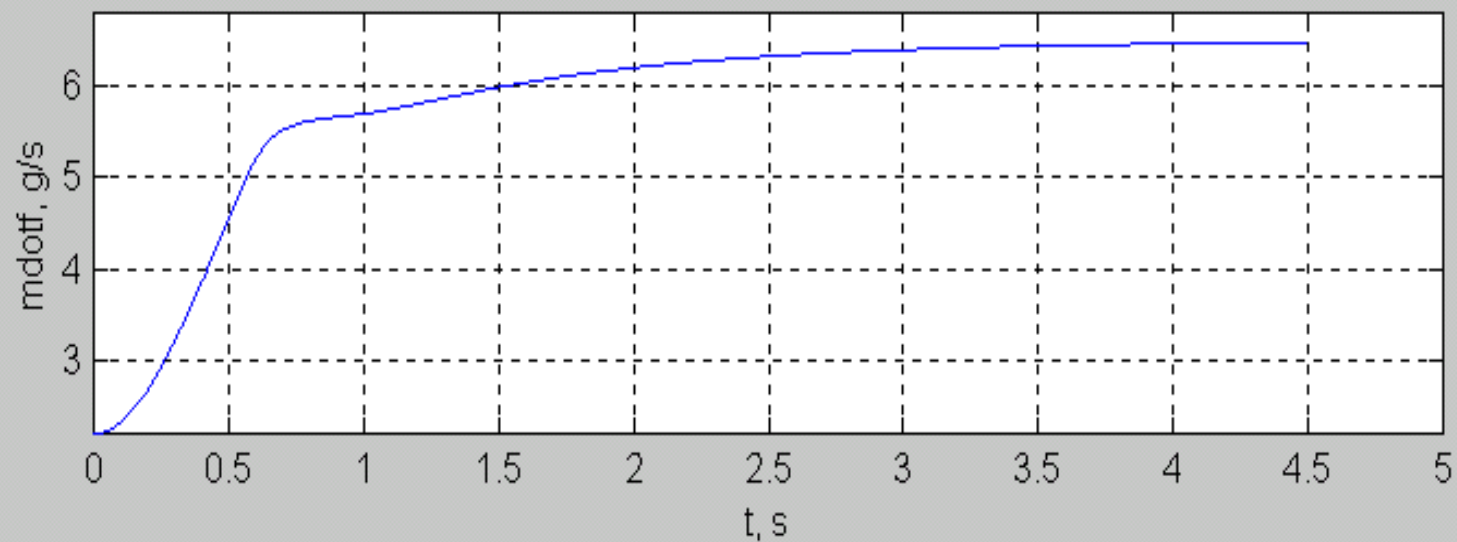
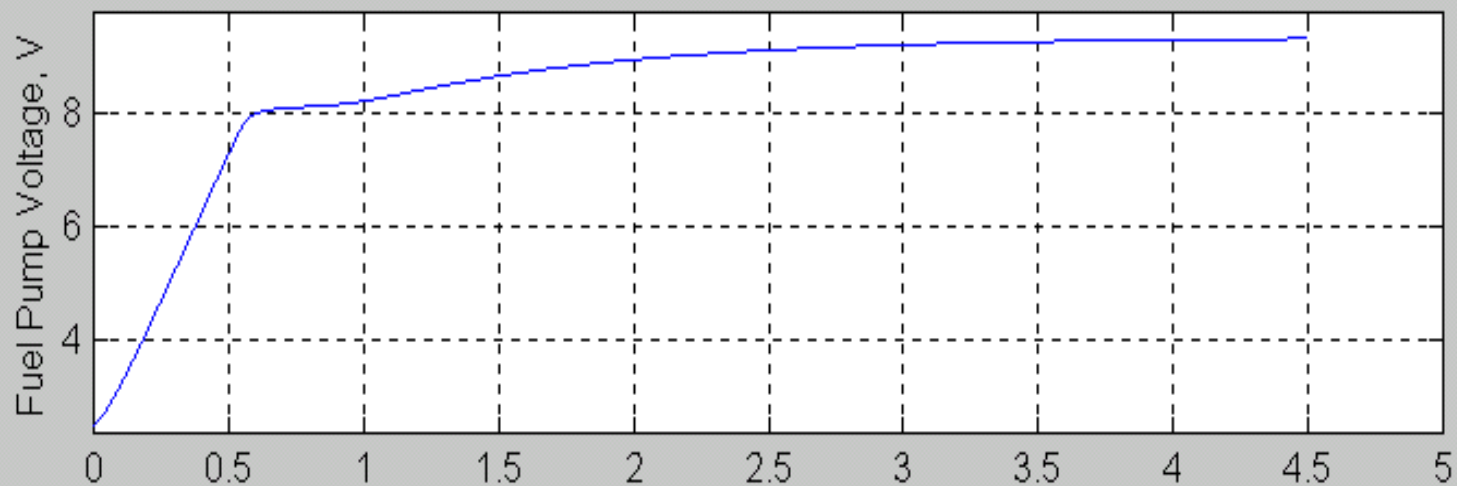
Ready



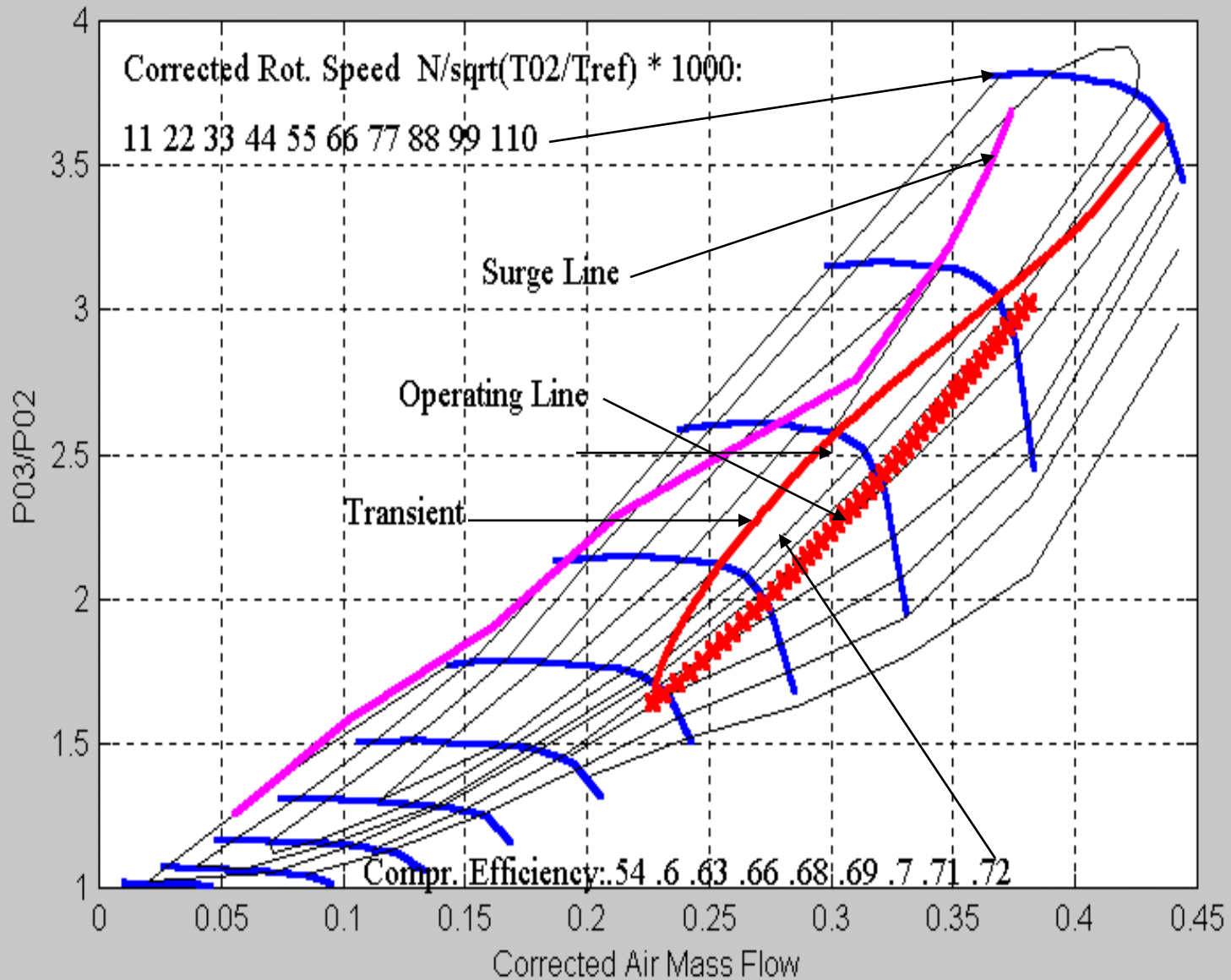
"MICROJET" FEED-BACK CONTROL. H= 1524m; M= 0.5.



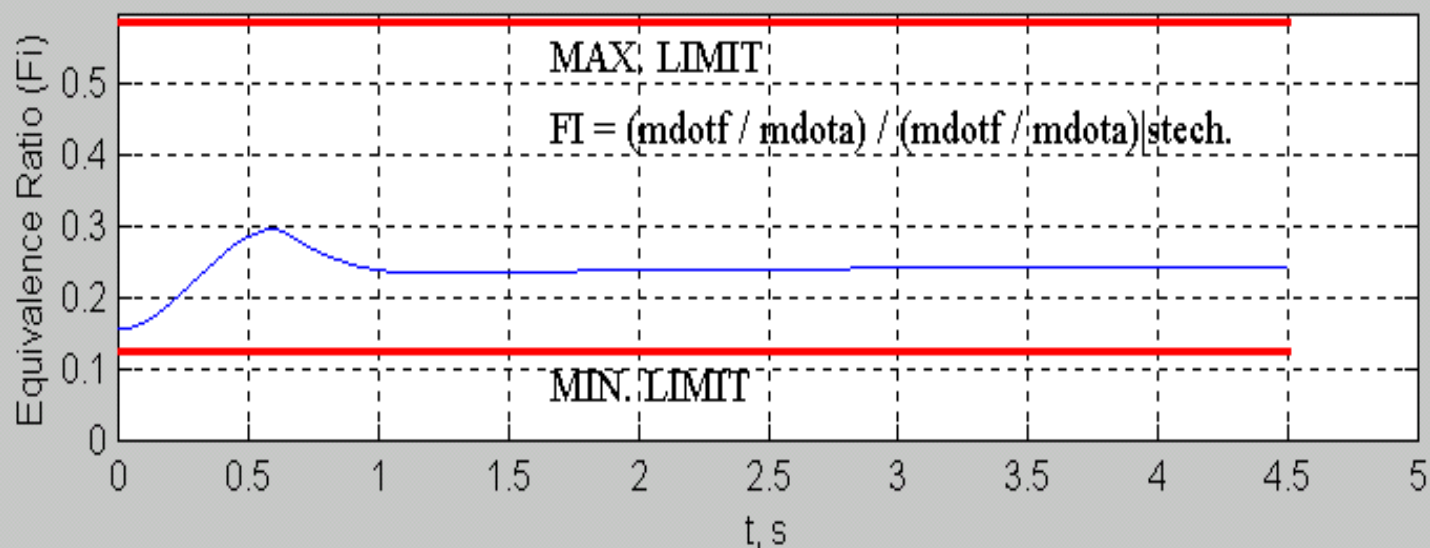
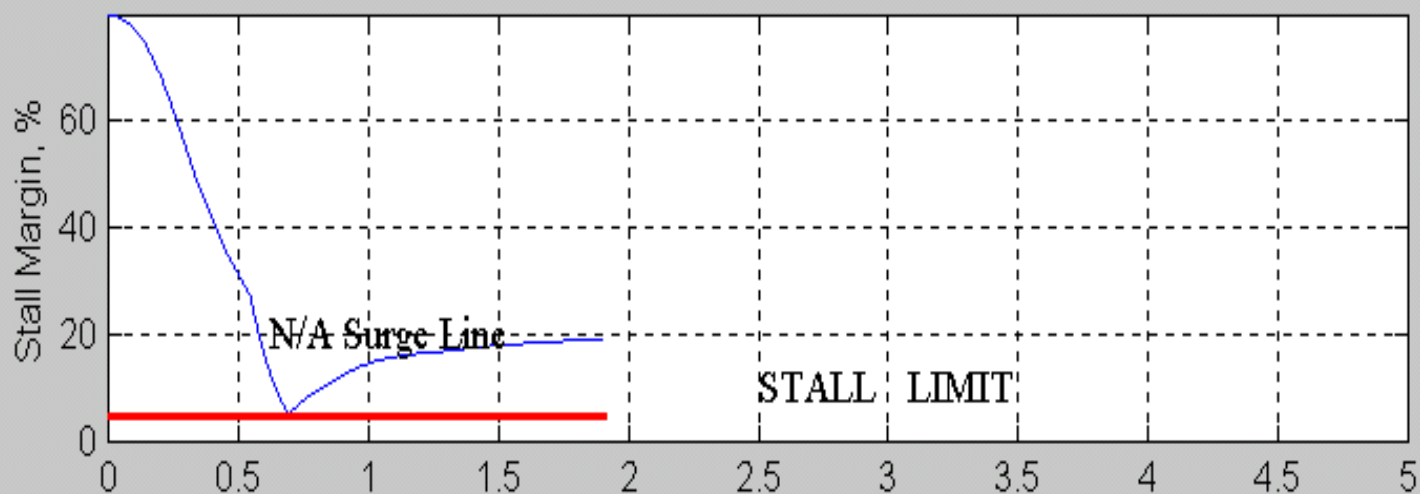
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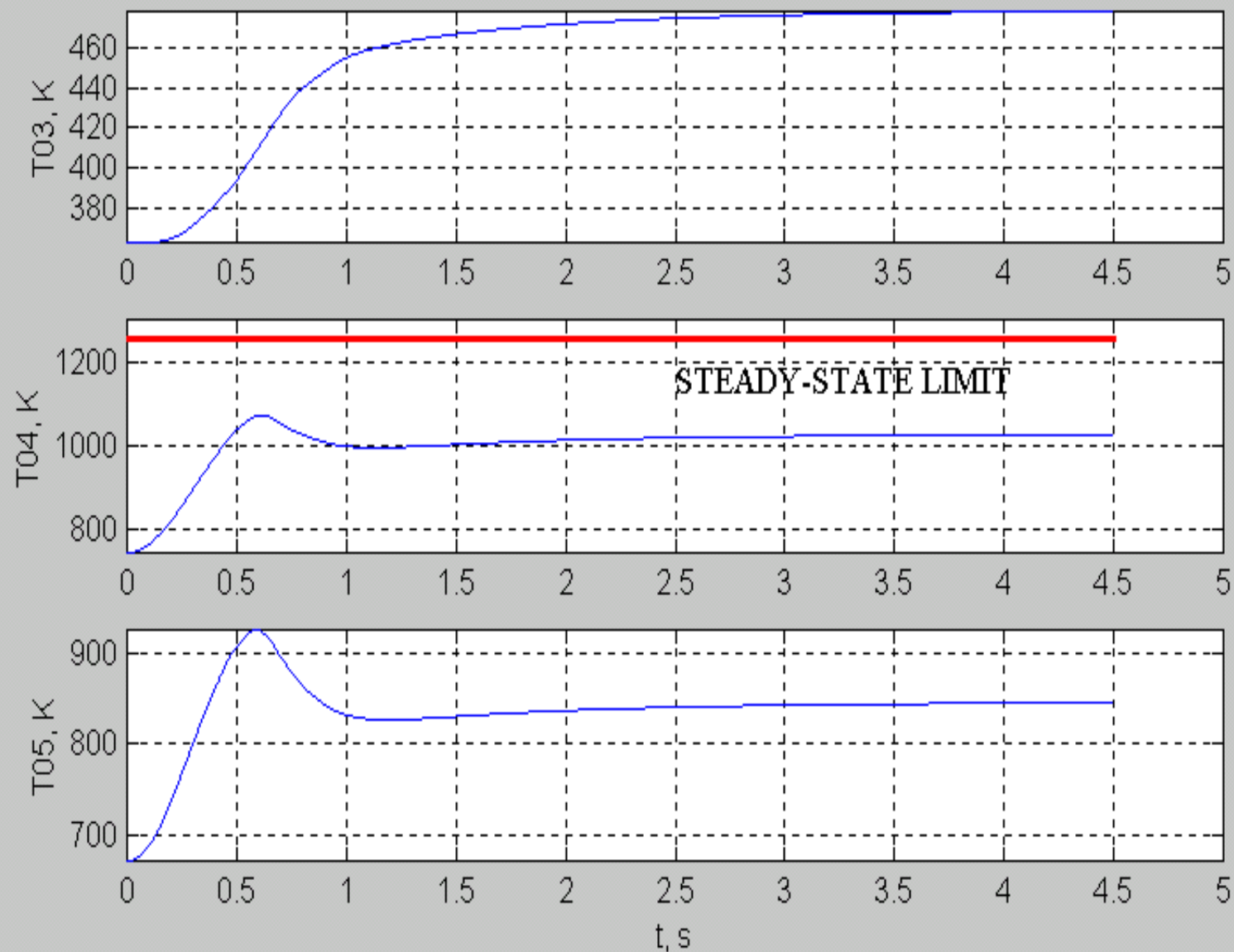
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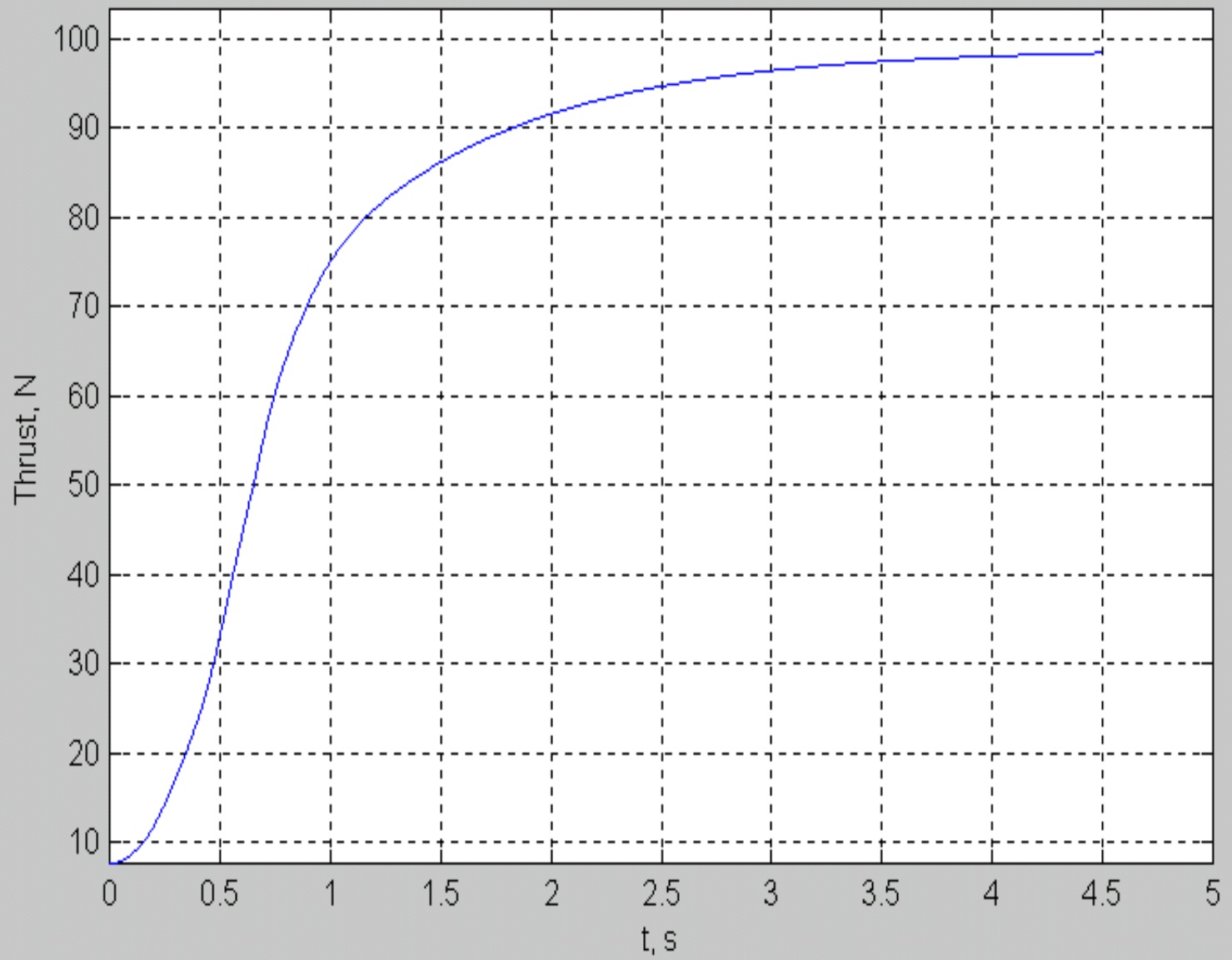
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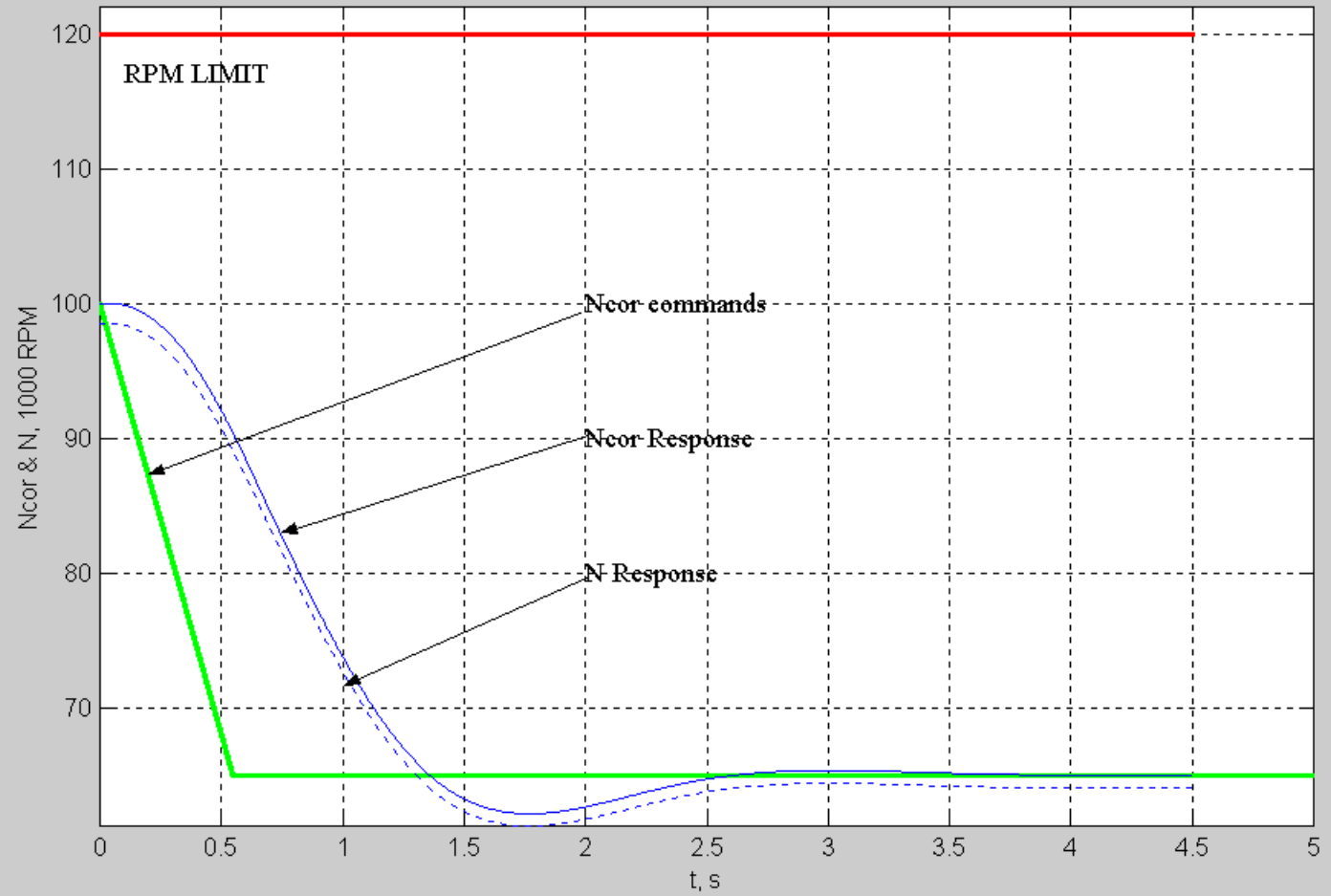
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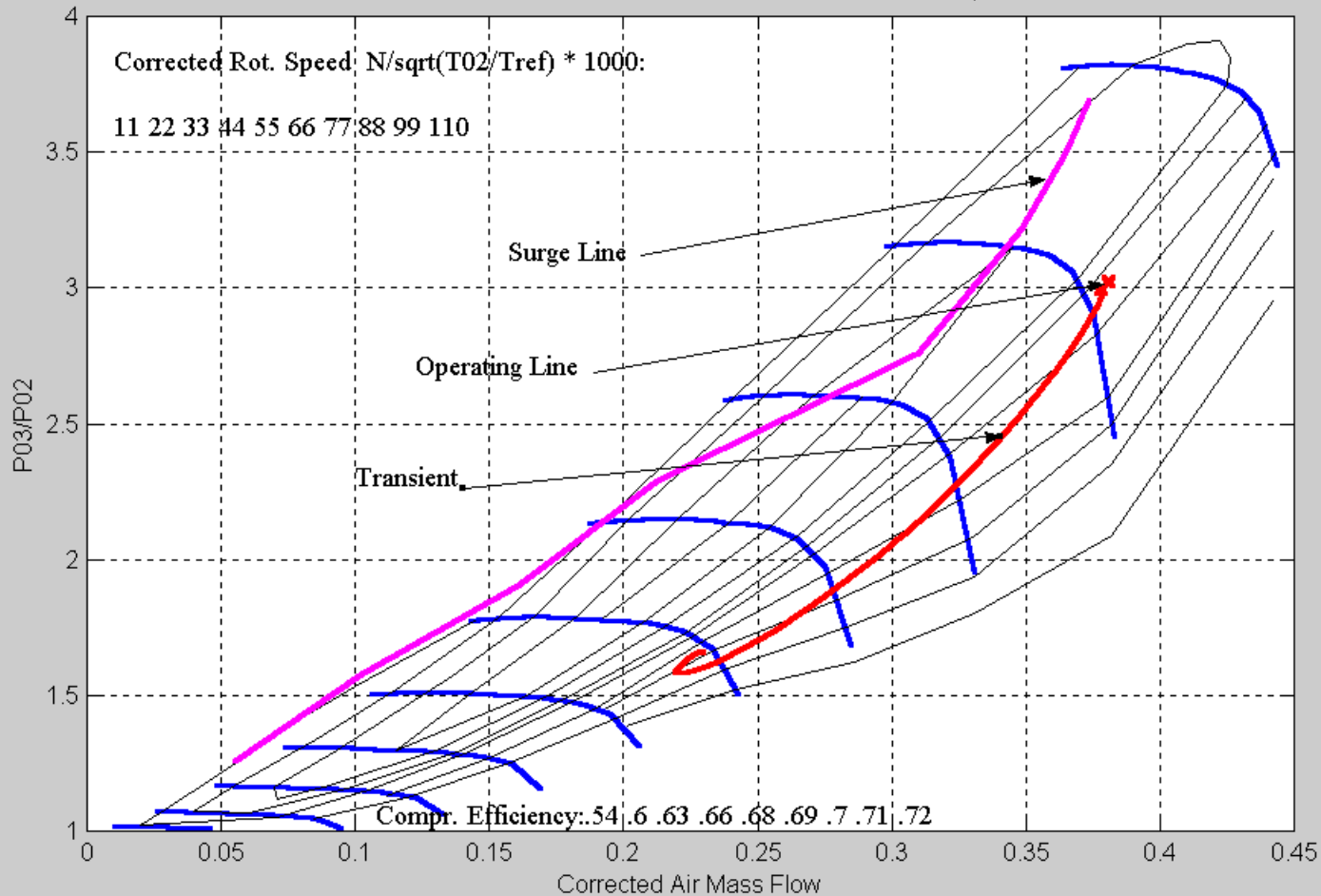
"MICROJET" FEED-BACK CONTROL. H= 1524m; M= 0.5.



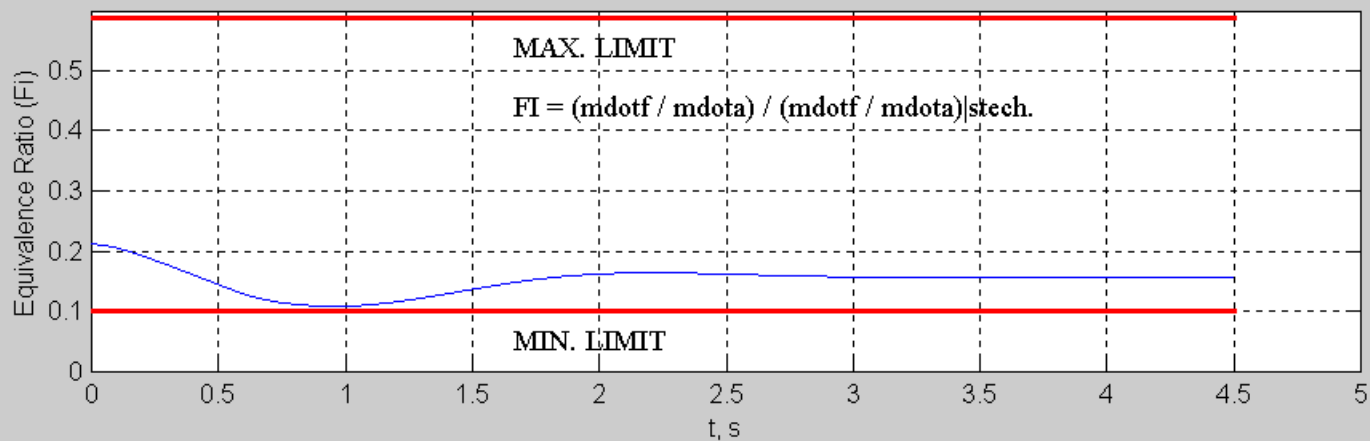
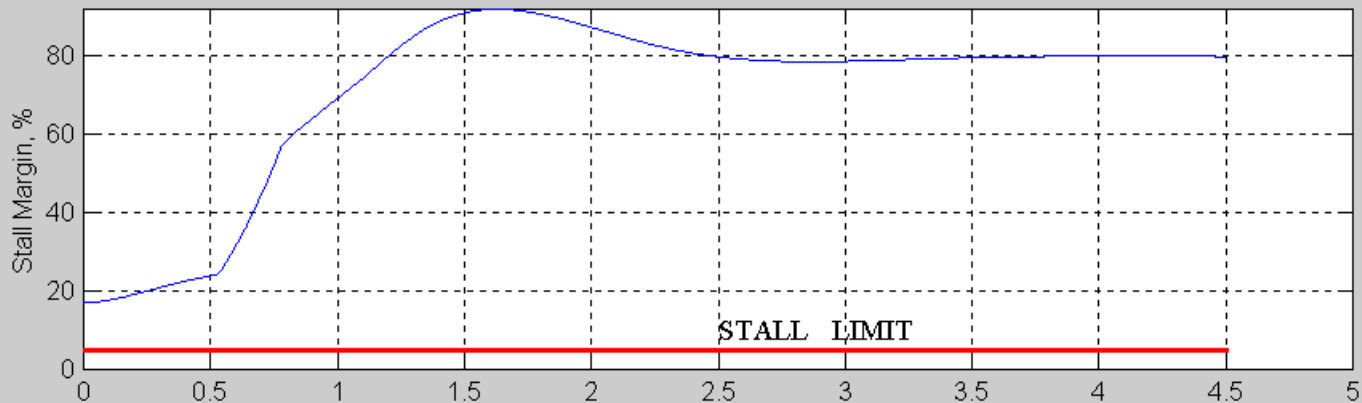
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"MICROJET" FEED-BACK CONTROL. H= 1524m; M= 0.5.



CONCLUSIONS:

- 1. DYNJET is a MATLAB/SIMULINK program for analysis of steady-state and dynamic performance of single-spool turbojet engine with convergent nozzle without afterburner**
- 2. DYNJET is a flexible program. It allows adding new functions and equations for investigation purposes**
- 3. Comparisons of simulation results with experimental data prove the model's validity.**
- 4. 100 computer simulations at flight conditions: $0 < H < 20000$ ft and $0 < M < 0.7$ prove the nonlinear controller corresponds to the specification requirements**